

Moment-Based Simulation of Microphysical Properties of Sulfate Aerosols in the Eastern United States: Model description, evaluation and regional analysis

Shaocai Yu*¹, Prasad S. Kasibhatla and Douglas L. Wright

Nicholas School of the Environmental and Earth Sciences, Duke University, Durham, NC 27708

¹Now is UCAR visiting scientist at Atmospheric Sciences Modeling Division (E243-01), National Exposure Research Laboratory, U.S. Environmental Protection Agency, Research Triangle Park, NC 27711.

Stephen E. Schwartz and Robert McGraw

Atmospheric Sciences Division, Brookhaven National Laboratory, Upton, NY 11973

Aijun Deng

Department of Meteorology, Pennsylvania State University, University Park, PA 16802

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* To whom the correspondence should be addressed: Phone: 919-541-0362
Fax: 919-541-1379, E-mail: yu.shaocai@epa.gov

ABSTRACT

A six-moment microphysics module for sulfate aerosols based on the quadrature method of moments has been incorporated in a host 3-D regional model, the Multiscale Air Quality Simulation Platform (MAQSIP). Model performance was examined and evaluated by comparison with the in-situ observations over the eastern US for 40-day period from July 19 to August 28, 1995. The model generally reproduces the spatial patterns (sulfate mixing ratios and wet deposition) over the eastern US and time series variations of sulfate mass concentrations. The model successfully captured the observed size distribution in the accumulation mode (radius 0.1 to 0.5 μm), in which the sulfate is predominately located, while underestimating the nucleation and coarse modes on the basis of the size distributions retrieved from the modeled six moments at the Great Smoky Mountains (GSM). This is consistent with better model performance on the effective radius (ratio of third to second moment, important for light scattering) than on number-mean and mass-mean radii. However, the model did not predict some of the moments well, especially the higher moments and during the dust events. Aerosol components other than sulfate such as dust and organics appear to have contributed substantially to the observed aerosol loading at GSM. The model underpredicted sulfate mixing ratios by 13% with about 50% of observations simulated to within a factor of 2. One of reasons for this underestimation may be overprediction of sulfate wet deposition. Sulfate mass concentrations and number concentrations were high in the source-rich Ohio River valley, but number concentrations were high also over the Mid-Atlantic Coast (New Jersey area). Most (77%) sulfate amount was below 2.6 km whereas most sulfate number (>52%) was above 2.6 km except over Ohio River valley (41%). These results demonstrate the accuracy, utility, practicality, and efficiency of moment-based methods for representing aerosol microphysical processes in large-scale chemical transport models.

1. Introduction

The sulfur cycle over North America has been simulated with regional and global 3-D chemical transport models (CTMs) by many investigators [Langner and Rodhe, 1991; Kasibhatla et al., 1997a; Benkovitz and Schwartz, 1997; Chin et al., 2000; Von Salzen et al., 2000; Rasch et al., 2000]. Most of these models have simulated only the mass concentration of sulfate aerosol and not size distributions. However, representing the microphysical properties of aerosols (i.e., their intensive properties [Ogren, 1995]) in addition to their mass concentrations (extensive properties) and understanding the influence of aerosol microphysical processes on properties of tropospheric aerosols are important because environmental effects of aerosols such as atmospheric visibility, climate change, acid deposition and health effects depend not just on the mass concentration but also on the size distribution and chemical composition of these particles [Sisler and Malm, 2000; Yu et al., 2000, 2001; Schwartz, 1996; Penner et al., 2002; Ghan et al., 2001]. Additionally, the mass loading of aerosols is itself influenced by processes whose rates depend on particle size. It is therefore necessary to include a microphysical representation of aerosol formation, evolution and removal processes in atmospheric CTMs. Most previous approaches to aerosol microphysical modeling have simulated the particle distribution function (PDF) either explicitly, by a bin-sectional approach [Whitby and McMurry, 1997; Russell and Seinfeld, 1998; Von Salzen et al., 2000; Jacobson, 2002] or by a multi-modal approach [Whitby and McMurry, 1997; Binkowski and Shankar, 1995; Wilson et al., 2001], in which particle size distributions are represented as the superposition of three lognormal subdistributions, or modes.

Recently, an alternative approach has been introduced that represents the aerosol in terms of the moments of the PDF [McGraw, 1997; Barrett and Webb, 1998]. The radial moments are defined as $\mathbf{m}_k = \int_0^{\infty} r^k f(r) dr$, where \mathbf{m}_k is the k^{th} radial moment, r is radius and $f(r)$ is the PDF for the number size distribution. The advantages of the method of moments (MOM) include comparatively straightforward implementation of the method as the moments evolve according to sets of differential equations having the same structure as the rate equations describing the evolution of reacting chemical species in the same background flow and freedom from errors associated with numerical diffusion in

particle-size space [McGraw, 1997]. Another advantage of MOM is the small number of variables required to represent aerosol properties; the six lowest-order radial moments directly give important aerosol properties: particle number concentration (n), particle mass concentration ($4\pi r^3 \rho_p / 3$; ρ_p is particle density), number mean radius ($r_n = m/n$), effective radius ($r_e = 3/2$), mass mean radius ($r_m = M/M$), and the standard deviation ($\sigma = [Mm - m^2]^{0.5}/m$) characterizing the width of the PDF [McGraw, 1997; Wright et al., 2000]. The more recently introduced quadrature method of moments (QMOM) [McGraw, 1997] overcomes closure difficulties inherent in the MOM and allows condensation and coagulation kernels of arbitrary functional form to be treated without a priori assumptions regarding the form of the PDF. The utility of MOM has been further enhanced by the development of methods such as Randomized Minimization Search Technique (RMST) and Multiple Isomoment Distribution Aerosol Surrogate (MIDAS), which use the first six moments to compute aerosol optical properties to within a 1-2% of those obtained directly from the PDF [Yue et al., 1997; Wright, 2000; Wright et al., 2002]. Even properties requiring integration over only a portion of the full size spectrum of the PDF such as cloud activation, or properties relevant to the PM 2.5/10 standards can be computed to an accuracy of about 10% or better [Wright et al., 2002].

Building on these developments in the MOM approach, we implement a six-moment aerosol microphysical module 6M [Wright et al., 2001] in a regional atmospheric chemical transport model (CTM), and use this newly-developed capability to simulate the summertime distribution of sulfate aerosols over the eastern US. Our focus on sulfate aerosols stems from studies which show that this is the dominant anthropogenic aerosol component in the eastern US [e.g. Sisler and Malm, 2000]. We present a detailed evaluation of model performance by comparing simulated particle mass and number concentrations, size parameters (effective radius, mass mean radius and number mean radius) and surrogates to the underlying size distributions with observations.

This work may be most closely compared to that of Von Salzen et al. [2000], who simulated the responses of sulfate aerosol size distributions over North America to SO_x emissions and H_2O_2 concentrations for 1994 summer and winter. Our study is distinguished from that of Von Salzen et al. [2000] in three important aspects: (i) the use of QMOM to simultaneously track the six lowest-order radial moments of a particle size

distribution; (ii) the evaluation of model performance against regional spatial and temporal variations of in-situ measurements for aerosol mass and number concentrations, and size parameters over eastern US; (iii) an analysis of regional budget of sulfate mass and number concentrations over the eastern US.

2. Model Description

The host three-dimensional regional CTM is the non-hydrostatic version of the Multiscale Air Quality Simulation Platform (MAQSIP) [Odman and Ingram, 1996]. MAQSIP is a prototype of US EPA Models-3 Community Multiscale Air Quality (CMAQ) Modeling System [Byun and Ching, 1999]. The model domain covers the eastern United State with a horizontal grid of 72x74 36-km grid cells (See Figure 1). The vertical resolution is 22 layers, which are set on a sigma coordinate, from the surface to ~160 hPa. The model was driven by meteorological fields from the MM5 meteorological model [Grell *et al.*, 1994]. The prognostic variables in the model are the gas-phase concentrations of SO₂ and H₂SO₄, and the first 6 radial aerosol moments. In the following sections, we describe the various components of the model as configured for this study.

2.1. Aerosol dynamics and microphysics

Aerosol microphysical processes are simulated using the module 6M [Wright *et al.* 2001] which is based upon the QMOM [McGraw, 1997] and MIDAS [Wright, 2000] techniques. The QMOM represents integrals over a size distribution using a set of abscissas and weights derived from the lower-order moments and requires no assumption about the distribution other than that it have well-defined moments. There are special cases where we assumed that the aerosol size distribution is log-normal. These are: (1) for primary emissions, and (2) for use with the cloud activation parameterization of Abdul-Razzak *et al* [1998]. However, the reasons for assuming a lognormal in these cases are not inherently related to the QMOM. Indeed we evolve six moments via the 3-point QMOM. For parameterization of a single lognormal distribution only three would have been required. By comparison with results obtained using a high-resolution discrete model of the particle dynamics, Wright *et al.* [2001] show that the accuracy of 6M is

good relative to uncertainties associated with other processes represented in atmospheric CTMs. Differences between 6M and the discrete model in the mass/volume moments and in the partitioning of sulfur (VI) between the gas and aerosol phases remain under 1% whenever significant aerosol is present, and differences in particle number rarely exceed 15% [Wright *et al.*, 2001]. Wright *et al.* [2001] have given a detailed description of the six-moment aerosol microphysical module. Here a brief summary relevant to the present study is presented.

Advection and diffusion processes operate on the dry (non-deliquesced) aerosol. The various processes in the aerosol module are performed (with operator splitting) in the order: primary emissions, water uptake, nucleation-condensation, coagulation, dry deposition, water release, and cloud processing. Primary (particulate) sulfate emissions are characterized in terms of moments by use of the lognormal distributions given in Whitby [1978] representing a power plant plume. Aerosol-water equilibration is assumed to be instantaneous, and water uptake and release with changing RH are calculated using a size-independent water uptake ratio, defined as $\mathbf{b}_{RH} = r_{wet}/r_{dry}$, computed from the data of Tang and Munkelwitz [1994] for $(\text{NH}_4)_2\text{SO}_4$. New particle formation via binary H_2O - H_2SO_4 nucleation is represented using the Jaeger-Voirol and Mirabel [1989] model, as parameterized in Fitzgerald *et al.* [1998]. The nucleated particles are produced at three discrete sizes (r_{n1}, r_{n2}, r_{n3}) with assumed relative weightings $(W_{n1}, W_{n2}, W_{n3}; W_{n1}+W_{n2}+W_{n3}=1)$, in analogy with the three quadrature abscissas and weights [Wright *et al.*, 2001]. For this application, $(r_{n1}, r_{n2}, r_{n3}) = (0.7 \text{ nm}, 3 \text{ nm}, 8 \text{ nm})$ and $(W_{n1}, W_{n2}, W_{n3}) = (0.33, 0.33, 0.34)$. We have not investigated the sensitivity of our model to nucleated particle size. However we expect little effect as the freshly nucleate particles are too small to contribute to the moments (other than particle number). Evidence for this is found in an early paper on the conventional MOM wherein the nucleated particles were assigned zero radius with negligible effect on the moments [McGraw and Saunders, 1984]. Nevertheless with the QMOM it appears necessary for numerical stability to assume a narrow distribution (for the freshly nucleated particles only) so as to get the initial quadrature points. This serves to get the evolution started, whereas for a monodisperse distribution the 3-point quadrature matrix would be singular. The

neutralization of H_2SO_4 is not explicitly modeled, and all H_2SO_4 is treated as ammonium sulfate immediately upon condensation.

The moment evolutions due to condensation, coagulation and dry deposition are done on the basis of the quadrature abscissas and weights. The moments evolve solely by evolution of the abscissas with the weights remaining constant under condensation growth, and by evolution of the weights with the abscissas remaining constant under dry deposition [McGraw and Wright, 2000]. The condensation rate is the modified Fuchs-Sutugin formula [Russell and Seinfeld, 1998; Kreidenweis et al., 1991], and the Fuchs kernel [Fuchs, 1964; Jacobsen et al., 1994] for coagulation is used. Dry deposition velocities have been calculated from the model of Giorgi [1986] for deposition to both ocean and land surfaces. The moment evolutions due to aqueous chemistry, rainout and washout during the cloud period are described in Section 2.4.

2.2. Transport and Emissions

The advection and vertical and horizontal diffusion schemes implemented in the MAQSIP are described by Odman and Ingram [1996]. While these schemes are suitable for chemical species, they cannot be applied to each of the moments because the moments of a PDF are not mathematically independent quantities. For example, the aerosol PDF is a positive definite distribution whose moments must satisfy certain convexity relations and moment inequalities [Feller, 1971]. The best known of these is Chebyshev's inequality $m - (m)^2 \geq 0$, but there are relations [Feller, 1971] connecting the higher order moments as well. Moment sequences can fail to satisfy these relations if advected independently, as advection algorithms in CTMs are only approximate. To overcome this limitation, inherent in most advection algorithms, we perform all aerosol mixing processes in such a way that moment sequences are advected as a whole. For this purpose a moment sequence may be viewed as a vector whose components are the moments themselves. This integral treatment of moment sets has been implemented by a "linear combination" approach whereby information is saved during the updating of particle number that is subsequently used to consistently update the higher moments as linear combinations of the moments in neighboring cells.

Emissions of gas-phase SO₂ and aerosol sulfate are prescribed in the model based on the 1990 EPA National Emissions Trends (NET90) Inventory. The number of layers used for emissions was limited to 14 (~2600 m) so as to not exceed a realistic maximum plume rise height [Houyoux *et al.*, 2000]. Figure 1 shows the distribution of summer SO_x (i.e., SO₂ + sulfate) emissions over the eastern US including both surface and elevated sources. Emissions occur mainly over the heavily industrialized Ohio River Valley and the Mid-Atlantic coast region. Approximately 98.8% (by mole) of the sulfur is emitted in the form of SO₂ and 1.2% in the form of SO₄²⁻. On the basis of the National Acid Precipitation Assessment Program (NAPAP) emissions inventory, Dennis *et al.* [1993] found that the fraction of sulfur emitted in the form of SO₄²⁻ ranged from 0.7 to 4.3% with a median of 1% for the eastern US. The emission fraction of SO₄²⁻ employed in this study is close to the median value of Dennis *et al.* [1993].

2.3. Sulfur Chemistry

The model includes a representation of gas-phase oxidation of SO₂ by OH as well as aqueous-phase SO₂ oxidation by H₂O₂ in cloud droplets. For OH and H₂O₂ concentrations, we use the prescribed hourly mean three-dimensional fields obtained from photochemical model calculations using the Carbon Bond Mechanism (version 4.2) [Gery *et al.*, 1989; Kasibhatla *et al.*, 1997b, 2000] with the same meteorology. Koch *et al.* [1999] explored the importance of using prognostic H₂O₂ by comparing results with those from a run having fixed H₂O₂ fields and found that the fixed H₂O₂ simulation had typically about 5% more sulfate at the surface, 5-10% less surface SO₂ and about 10% greater deposition flux. The rate constant for SO₂ oxidation by OH is taken as 1.0x10⁻¹² cm³ molecule⁻¹ s⁻¹. As this rate can vary with the temperature, the oxidation rate of SO₂ by OH calculated according to the method of Demore *et al.* [1992] will be added in the future work. Following Kasibhatla *et al.* [1997a], we use a simplified H₂O₂ limitation scheme for the in-cloud oxidation of SO₂ by H₂O₂. Specially, we assume that if the H₂O₂ concentration within the grid box is greater than the SO₂ concentration, all SO₂ within the grid box is converted to sulfate, otherwise the amount of SO₂ converted to sulfate is set equal to the amount of H₂O₂ within the grid box.

2.4. Cloud Processes

2.4.1. Cloud scheme

The cloud types in the MAQSIP are sub-grid convective cloud (precipitating and non-precipitating) and grid-scale resolved stratiform cloud. The resolved and sub-grid cloud modules were derived from the mesoscale model [MM5, *Grell et al.*, 1994] and the diagnostic cloud model in the Regional Acid Deposition Model (RADM) version 2.6 [*Chang et al.*, 1987, 1990; *Dennis et al.*, 1993; *Walcek and Taylor*, 1986], respectively. *Dennis et al.*, [1993] discussed the limits of the simplified convective model originally conceived for the RADM and corrections to the RADM (version 2.6). As the resolved clouds are large-scale and always occupy the full grid box, we take them as stratiform. The sub-grid clouds modeled in RADM are convective and taken as cumulus. The non-convective and convective precipitation amounts output from MM5 were used to drive the resolved cloud and subgrid precipitating cloud respectively in MAQSIP. This means that only total precipitation amounts at the first layer (surface) are available but not data for each layer and that the sub-grid precipitating clouds are simulated only when the MM5 indicates precipitation from its convective cloud model. In this study, we distributed the total precipitation amount to each vertical cell on the basis of a weighting function calculated according to the available information from output of MM5 as described in Appendix A. With the precipitation rate at each layer, and the condensed cloudwater and rainwater reported by MM5, the resolved cloud model evaluated aqueous chemical reactions and wet deposition using the procedure described in Section 2.4.2. For resolved clouds, their lifetimes were assumed to vary on the basis of the time step of the model. This means that the effect of the resolved clouds on species concentrations was calculated at each time step of the model although the meteorological driver (MM5) gave hourly output for the resolved clouds. The parameters for the resolved clouds at each time step (<1 hour) in this model were interpolated on the basis of the hourly output from the MM5. For all sub-grid clouds, a 1-hour lifetime has been assumed and the influence of sub-grid clouds on the species concentrations was calculated once an hour. The cloud fraction calculations for the sub-grid cloud depend on cloud types and have been described thoroughly by *Dennis et al.* [1993].

2.4.2. Cloud processing for aerosol evolution and wet deposition

When the meteorological driver indicates cloudy air is present, the aqueous chemistry routine uses gas-phase SO_2 and H_2O_2 concentrations to calculate the total amount of sulfate produced in the limiting reagent approach as described in Section 2.3. When cloud is formed in an air parcel, the MOM must partition the aerosol into activating and interstitial portions, and characterize each portion by a set of moments. To perform this partitioning and apportion sulfate mass among the cloud drops, we first estimate cloud droplet number by using the aerosol activation parameterization method of *Abdul-Razzak et al.* [1998], which implicitly accounts for control of maximum supersaturation by aerosol concentration and size distribution. For a single aerosol type, this parameterization method requires characterization of the aerosol PDF in terms of a lognormal distribution. The lognormal parameters N , r_g and σ_g can be obtained algebraically from any three of the six moments; m_0 , m_1 , and m_2 are used here. The activated fraction (N_c/N) of the aerosol is estimated with the activation parameterization method and then cloud droplet number is calculated with activated fraction and particle number. A MIDAS surrogate to the unknown PDF is retrieved from the six moments. The particle radius ($r_{c,\text{eff}}$), from which to infinity integration of the surrogate PDF yields a number of particle equal to the estimated cloud droplet number, can be found. With this $r_{c,\text{eff}}$, we partition the surrogate PDF into activating and interstitial portions. Then the moments of the interstitial aerosol are calculated with the surrogate PDF from 0 to $r_{c,\text{eff}}$, and subtracting these moments from the total moments yields the moments of the activating portion of the aerosol. In view of the extreme narrowing of cloud drop size distributions relative to the size distribution of the activated particles, and because aqueous reaction rates within clouds are to good approximation proportional to cloud drop volume, we apportion the sulfate formed by aqueous-phase reactions equally among the activated particles. A more detailed description is given in Wright et al. [2001]. After evolution of the activated aerosol, the moments of these two portions of the aerosol are summed to give the moments of the total aerosol at the end of the time step.

The wet deposition rates are due to two processes: rainout (in-cloud scavenging) and washout (below-cloud scavenging). In this study, both processes are treated as first-order loss and simultaneous processes without operator splitting. For aerosols, washout

coefficient depending on retrieved r_g and \mathbf{S}_g was computed on the basis of calculations of *Dana and Hales* [1976] for mass washout coefficients (Figure 2 of *Dana and Hales* [1976]) with the 4th-order polynomial equation. Again the lognormal parameters N , r_g and \mathbf{S}_g are obtained from moments: \mathbf{m}_0 , \mathbf{m}_1 , and \mathbf{m}_2 . SO_2 is partitioned according to Henry's Law between the gas-phase, the cloud water, and the rain water from above that will pass through the cell during the time step. H_2SO_4 and sulfate aerosol are assumed to be completely in the aqueous phase, and partitioned between the cloudwater and rainwater according to their relative amounts. Details on calculation of wet deposition rates (rainout and washout) for SO_2 , H_2SO_4 and sulfate aerosols are described in Appendix B. As the resolved clouds are large scale and always occupy the full grid box, we take them as stratiform. The sub-grid clouds modeled in RADM are convective and taken as cumulus. The basic approach within the aerosol module is to run independent, concurrent simulations for three sets of conditions: (1) the appropriate clear-sky conditions, (2) the conditions for cumulus clouds as indicated by the sub-grid cloud module, and (3) the conditions for stratiform clouds as indicated by the resolved-cloud module. The results for the moments are then updated by forming a linear combination of the results obtained for the three independent simulations using the fractional cloud cover for each cloud type. It sometimes occurs in the model that even when a resolved cloud is specified by the meteorological preprocessor (MM5) to be present throughout the entire grid cell (cloud-cover fraction equal to unity), the sub-grid convective cloud module (RADM) will also create a non-precipitating cloud for some fraction of the grid cell volume. When this occurs these cloud-cover fractions are rescaled until their sum is unity. These rescaled cloud-cover fractions are then used in forming the linear combinations used for updating the moments and sulfuric acid vapor concentration, as described previously.

2.5. Base case and sensitivity studies.

Model runs were carried out for a base case and for three sensitivity studies:

- (1) Case 1: Base case

In this case, the model considers all processes as described above and the fraction of sulfate (include mass and all moments) taken into rain and cloud water was 100% during cloud periods. We refer this case as “100%” scavenging case and base case.

(2) Case 2: “50%” scavenging case

As case 1, but only 50% of sulfate was taken into rain and cloud water during the cloud process. Measurements of the chemical composition of the liquid water and interstitial air in warm, non-precipitating strat-cumulus clouds at various locations in the eastern US, *Daum et al.* [1984a, b] showed that the peak of the distribution of scavenging efficiencies for SO_4^{2-} was at a lower value (0.6-0.8) than for H^+ and NO_3^- , and a substantial number of samples exhibited values of scavenging efficiencies that were less than 0.5. As recommended by Daum (*P. Daum*, 2001, personal communication) on the basis of their measurements, the fraction of sulfate taken into cloud water during the cloud process is taken as 50%. The 50% scavenging efficiencies are applied uniformly to all six moments. We refer this sensitivity case as “50%” scavenging case. Comparisons of simulation results of “100%” and “50%” cases permit examination of sensitivity of the simulation results to fractional uptake.

(3) Cases 3 and 4: doubling the condensation rate

In these sensitivity studies, we doubled the condensation rate of H_2SO_4 onto the sulfate aerosol for both “50%” and “100%” cases to account for condensation onto other aerosols. As fine particle mass concentration over the eastern US is about 60% sulfate [*Sisler and Malm*, 2000], this may account for the effect of other aerosols (organics, seasalt, dust and others) under assumption that other aerosols provide aerosol surface area for condensation equal to that of the sulfate aerosol. This reduces the concentrations of gaseous sulfuric acid and hence the rates of nucleation and coagulation.

2.6. Retrieval of modeled size distributions

The modeled size distributions were retrieved by the Randomized Minimization Search Technique (RMST) [*Yue et al.*, 1997; *Wright et al.*, 2002] on the basis of the six moments from the model. In the RMST retrieval, we used 19 nonuniform bins with

radius boundaries of 0.01, 0.02, 0.03, 0.04, 0.05, 0.06, 0.07, 0.085, 0.10, 0.125, 0.15, 0.20, 0.25, 0.35, 0.45, 0.60, 0.75, 1.00, 1.25 and 1.75 μm . The last 15 bin structures of the RMST retrieval are chosen to be the same as those of a Passive Cavity Aerosol Spectrometer Probe (PCASP). The basic idea of RMST is to find a retrieved size distribution (19 size bins) whose calculated six moments have a minimum deviation from the modeled six moments. The bin structure, number of bins, number of solutions, and convergence tolerance are the most important parameters. In this application, the retrieved size distribution is obtained by averaging 20 solutions with 1% tolerance.

3. Simulation of sulfate aerosols and model evaluation over the eastern US

The sulfate aerosol concentrations and size distributions over the eastern US strongly depend on the emissions and chemical-physical atmospheric processes. Over the eastern US, the surface sulfate concentrations show a strong seasonal cycle with maxima in the summer and minima in the winter [Shaw and Paur, 1983]. The simulation results of Kasibhatla *et al.* [1997a] found that the column SO_4^{2-} burden over the eastern North America was $\sim 15 \text{ mg m}^{-2}$ in summer, much higher than that in winter ($\sim 6 \text{ mg m}^{-2}$) because of increased photochemical production of oxidants. As sulfate is the most important component of aerosols and sulfate aerosol concentrations (both natural and anthropogenic) are the greatest over the eastern US in summer, the ability to simulate the variability in sulfate aerosol properties during the summer will provide a good test for the performance of the model.

3.1. Measurements used for model evaluation

A comprehensive performance evaluation of the aerosol module in a 3-D air quality model requires an extensive dataset on aerosol properties. The Southeastern Aerosol and Visibility Study (SEAVS) measured sulfate mass concentration, aerosol number concentration and size distributions at the Great Smoky Mountains (GSM) National Park during July and August, 1995 [Andrews *et al.*, 2000; Ames *et al.*, 2000]. To use this dataset, we have run the 40-day simulation from 12:00 (GMT) 19 July to 12:00 (GMT) 28 August 1995. These measurements and four other data sets suitable for model evaluation during this period are briefly described below.

The datasets for the sulfate aerosols are as follows: (1) data from the SEAVS experiment conducted from July 15 through August 25, 1995, at Look Rock Ridge (84 W, 36 N; elevation 900 m) at the GSM [Andrews *et al.*, 2000; Ames *et al.*, 2000]. The mean sulfate mass concentrations were determined using Teflon filter as a collection method with inlet size cuts of 2.1 μm (IMPROVE sampler) over 12-hr daytime sampling periods (7:00 a.m. to 7:00 p.m. EDT) [Ames *et al.*, 2000]. The aerosol number size distributions between 0.05 and 1.25 μm radii with 34 bins were determined by an Active-Scattering Aerosol Spectrometer (ASASP-X) with a sampling time of at least 15 min [Ames *et al.*, 2000; S. Kreidenweis, R. Ames and J. Hand, private communication, 2002]. If more than one measurement was available in an hour, the first measured size distribution was used to represent the measurement in that hour. A Total of 105 observed size distributions, with RH<40% to represent the dry aerosols [Ames *et al.*, 2000], were used to compare with the model results. Note that by assuming that the aerosol is always dry at RH<40%, we will sometimes underestimate particle size at low RH. (2) The observed sulfate mass concentrations from the Clean Air Status and Trends Network (CASTNET, Holland *et al.*, 1999). Teflon filters were normally exposed for 1-week intervals (Tuesday to Tuesday) to collect aerosol for sulfate mass concentration analysis. (3) The observed sulfate mass concentration data from the IMPROVE program. Two 24-hour samples were collected on Teflon filters each week, on Wednesday and Saturday, beginning midnight local time [Sisler and Malm, 2000]. (4) Vertical profiles of the aerosol number size distributions determined during the Southern Oxidants Study (SOS). Size distributions for particle radii in 15 size-bins between 0.05 and 1.75 μm were determined by a Passive Cavity Aerosol Spectrometer Probe (PCASP) over Nashville, Tennessee from June 24 to July 20, 1995 [Hubler *et al.*, 1998]. (5) The aerosol size distributions at Black Mountains (35.66 N, 82.38 W, elevation 951 m), Mt. Mitchell State Park, North Carolina. Size distributions between 0.008 to 0.3 μm radii with 50 size-bins were determined by the TSI Differential Mobility Particle Sizer (DMPS) [Yu *et al.*, 2000, 2001]. As heating was applied to the aerosol sampled by the PCASP and DMPS, it is assumed that the results are representative of the dry aerosol size distributions. The sulfate mass concentrations were calculated on the basis of assumption that particles were composed of ammonium sulfate. SO₂ mixing ratios are also available in the above

studies except those on Black Mountain. Observations at sites which were not classified as rural sites or were not located at least 5 grid boxes from the nearest model boundary were excluded. In some small cases where two or more stations were located in a single grid cell, the mean observation was used.

For the comparison of wet sulfate deposition, two data sets from the National Atmospheric Deposition Program (NADP, see *Lynch et al.*, 1995) and EPA CASTNeT [*Holland et al.*, 1999] are used. Both NADP and CASTNeT measure sulfate wet deposition with weekly resolution (starting and ending at 0900 (local time) on Tuesdays). In summary, the observed sulfate mixing ratios at 60 stations, SO₂ mixing ratios at 45 stations and wet sulfate deposition at 117 stations were used to evaluate the performance of the model over the eastern US. Reported concentrations of sulfate and SO₂ in air were converted from the original units to mixing ratios in units of parts per billion (ppb = nmol per mol air) as this quantity has the advantage of being independent of pressure and temperature [*Schwartz and Warneck*, 1995]. Figure 2 shows the locations of the stations whose observations were used in this study over eastern US.

3.2. Initial and boundary conditions

The model was initialized by using model itself to generate initial conditions. First, mixing ratios of gaseous SO₂, and H₂SO₄ for all cells were set to 10⁻³ and 10⁻⁴ ppb respectively, and the six moments of aerosol size distribution for all cells were calculated according to the results for the marine background aerosol case from Table 7.3 of *Seinfeld and Pandis* [1998], i.e. $N_1=133 \text{ cm}^{-3}$, $D_{p1}=0.008 \text{ m}$ (geometric mean diameter), $\ln(\mathbf{s}_{g1})=0.657$ (geometric standard deviation); $N_2=66.6 \text{ cm}^{-3}$, $D_{p2}=0.266 \text{ m}$, $\ln(\mathbf{s}_{g2})=0.210$; $N_3=3.1 \text{ cm}^{-3}$, $D_{p3}=0.58 \text{ m}$, $\ln(\mathbf{s}_{g3})=0.396$. Under the assumption that the aerosol consisted of ammonium sulfate, the sulfate mixing ratio was 0.42 ppb for this marine background aerosol case. The boundary conditions were the same as these initial conditions. The model was run for the 40-day period (12:00 (GMT) 19 July to 12:00 (GMT) 28 August, 1995) with the MM5 meteorological conditions. Then we used the results of 40-day simulation as the initial conditions for the next 40-day simulation and the boundary SO₂ mixing ratio was set to 0.17 ppb for this new run. This approach was

taken so as not to bias the model to low concentration that would result if the model run were initialized with low background concentrations.

3.3. Evaluation of model and discussions

3.3.1. Time-series comparisons at the Great Smoky Mountains (GSM) and at the Black Mountain, North Carolina

This section compares time-series of modeled and observed moments, mass concentration and size parameters. Figure 2 shows the time-series of observed and modeled sulfate mass and the synoptic conditions at the GSM location during the SEAVS period [Sherman *et al.*, 1997; Ames *et al.*, 2000]. The dominant synoptic feature during this period was Hurricane Erin, which made landfall around August 2, 1995. As shown in Figure 2c, the model captured the buildup of observed sulfate mass from August 9 to 13, a dip during August 15-16, and a peak during August 17-18. However, the model underpredicted slightly sulfate mass peak after the Hurricane and overpredicted slightly the sulfate mass concentrations before and during the Hurricane Erin (Figure 2c).

For comparison of aerosol number concentration, moments and size parameters, one should bear in mind that the model simulates sulfate only whereas the observed moments and size distributions are for all aerosol species. Figure 3 shows that there were large variations of observed six moments at the GSM during the SEAVS period. The observed moments except m_0 were very high during the dust (July 23 to 26) and peak (August 13 to 19) periods, especially for m_1 and m_2 , when compared to other periods. As compared to the observations in Figure 3, the model generally performs much better on the low moments (m_0 , and m_1) than high moments (m_2 and m_3) at the GSM. The mean modeled number concentrations are 1516 cm^{-3} for the base case, somewhat higher than the mean observed number concentration (1139 cm^{-3}). The measurements determined the number size distributions only between $0.05 \text{ }\mu\text{m}$ and $0.125 \text{ }\mu\text{m}$, leading to possible underestimate of the actual number concentration (zeroth moment). The first panel of Figure 4 for the number concentration (m_0) shows that the model has similar magnitude to the observations and captured the increase trends of the observed number concentrations during August 10 and August 17 at the site. The model seriously underpredicts the high moments, especially for m_2 and m_3 , during the periods of dust (July 23 to 26) and high

concentrations (August 13 to 19). These underpredictions are attributed to the contributions of large particles of aerosol species other than sulfate in the observed particles as analyzed below. The soil mass concentration of the fine aerosol (diameter < 2.5 μm) was the highest for the whole study during the dust event, indicating the likely presence of large particles [Sherman *et al.*, 1997]. The OC concentrations increased dramatically during the transition and peak period (July 8-18).

The number concentrations and number mean radii are determined mainly by the particles at the small size range (nucleation mode) whereas effective radii and mass mean radii are determined mainly by the particles at the large size range (accumulation and coarse modes). For example, Woo *et al.* [2001] found that approximately 89% of the total number of particles were found to be smaller than 0.05 μm radius, and 26% were found to be smaller than 0.005 μm radius on the basis of aerosol size distributions in 0.0015 to 1.0 μm radius range measured every 12 minutes for 24 months beginning August 1998 in Atlanta, GA. Therefore, it is extremely difficult to simulate the number concentrations and size distribution, and this is a big challenge for modeling aerosol evolution. The work of Whitby [1978] demonstrates the strong tendency for the nucleation, accumulation and coarse particle modes to separate when the particle distribution function is transformed in terms of number, surface area and volume coordinates. Specifically, the nucleation mode is revealed on a number distribution plot, the accumulation mode on a surface area distribution plot, and the accumulation and coarse modes, which make similar but separate contributions, on a plot of the particle volume distribution. The radial moments for each of these transformed distributions are given in terms of moment ratios that utilize just the four lowest-order radial moments of the original (untransformed) particle distribution function. These are the number mean radius ($r_n = \bar{m}/\bar{n}$), the surface area mean radius (\bar{a}/\bar{n}), which equals effective radius (r_e), and volume mean radius (\bar{v}/\bar{n}), which equals mass mean radius (r_m). Taken together, these moment ratios provide a powerful, targeted indicator of model performance for representing the different Whitby modes. Figure 4 shows the time-series of modeled and observed these moment ratios (r_e , r_n and r_m) at the GSM during the SEAVS. The observed r_n values are systematically higher than the modeled values over the whole period and the observed r_m values are also systematically higher than the modeled values

during the dust and peak periods when other aerosols made a substantial contribution to the entire aerosols (Figures 2a, b). In contrast, both mean modeled r_e (0.159 μm) and size standard deviation s (0.050 μm) were close to the observations ($r_e=0.155$ μm and $s=0.039$ μm) as indicated the time-series of Figure 4. This is in agreement with the expectation that the sulfate model provides a good representation of the accumulation mode and most of surface areas of the particles have been represented by the modeled sulfate as indicated below.

The modeled size distributions were retrieved by the RMST [Yue *et al.*, 1997; Wright *et al.*, 2002] on the basis of the corresponding six moments from the model. Figure 5 shows comparisons of modeled and observed size distributions for some cases at the GSM. Note that ASASP-X measured aerosol number size distributions only between 0.05 and 1.25 μm radii. As can be seen, the model successfully captured the observed size distributions in the accumulation mode between 0.10 and 0.40 μm radii, with some underestimates especially for large particles (radius >0.5 μm) and small particles (radius <0.1 μm). It should be recalled, however, that the sulfate is expected to exhibit dry radius smaller than 0.5 μm , whereas the particle radii are expected to be dominated by other species. This may account for the departure above this radius. This is in agreement with the recent modeling study of global mixed aerosol fields of Wilson *et al.* [2001], who found that the accumulation mode at the surface is dominated by the sulfate mode in the continental areas.

The observed small particles (radius <0.1 μm) and large particles (radius >0.5 μm) undoubtedly include the contributions of aerosol substances other than sulfate. There were significant other aerosol components at the GSM during SEAVS period as shown in Figure 2a and 2b [Sherman *et al.*, 1997]. The mean concentrations of $\text{PM}_{2.5}$, $(\text{NH}_4)_2\text{SO}_4$, inorganics, OC, EC, CI and soil were 25.38, 9.40, 11.28, 2.98, 1.08, 0.04 and 1.47 g m^{-3} respectively. This indicates that ammonium sulfate and TOC (OC+EC) contributed 37% and 16% for $\text{PM}_{2.5}$ mass respectively at the GSM during the SEAVS (Figure 2a and 2b). This points out the important contributions of non-sulfate aerosols to the observed particles. Nucleation events apparently attributable to organics have been frequently observed in the forested region [Kulmala *et al.*, 1998; Kavouras *et al.*, 1998] and

industrialized agricultural regions [Birmili and Wiedensohler, 1998]. In the chemical analysis of the particles smaller than 0.25 μm radius in connection with the increase of the Aitken nuclei over a forested area, Kavouras *et al.* [1998] found the existence of organic acids (such as pinonic, formic and acetic acids), which are formed as oxidation productions of gaseous monoterpenes emitted by the forest. The importance of the anthropogenic hydrocarbons in the formation of secondary organic aerosol was also emphasized by Odum *et al.* [1997]. Organics have been found to contribute substantially to aerosol optical depths over the eastern coast of US [Hegg *et al.*, 1997]. The results of Figure 5 can be interpreted as suggesting the presence of non-sulfate particles in both radius $<0.1 \mu\text{m}$ (nucleation mode) (perhaps organics, which are heavy in the region as shown in Figure 2b) and radius $>0.5 \mu\text{m}$ (perhaps organics and soil) that are not included in the sulfate model. This is consistent with the previous analyses for the moments in Figure 3 and size parameters in Figure 4. Discrepancy between model and observations might also arise from inaccuracy in the treatment of nucleation and of primary sulfate emissions.

Figure 6 shows the time-series of modeled and observed six moments at Black Mountain, North Carolina, during August 15-28, 1995. The model captures the general magnitudes of observed six moments with better performance on μ_1 and μ_2 . There are similar explanations for the discrepancy between the model and observations for size parameters at Black Mountain as those at GSM when we retrieve the size distributions on the basis of the modeled six moments (not shown). Note that the TSI DMPS measured aerosol particles only over the radius range from 0.008 to 0.3 μm at Black Mountain as mentioned before, and the Black Mountain site (36 N, 82 W) is close to the GSM (36 N, 84W).

3.3.2. Comparisons with the regional observations and wet deposition over the eastern US

Figure 7a shows the spatial distribution of ratios of modeled to observed mean values at each station during the 40-day simulation over the eastern US for the base case. The model overestimated the SO_4^{2-} mixing ratios in some stations of the Southeast but underestimated them in all stations of the Northeast. For the 50% case, the

underestimation of sulfate mixing ratios in the Northeast was improved but the overestimation of sulfate mixing ratios in Southeast was increased (Figure 7b). Figure 8 shows scatter plots of model versus the individual concentration measurements for sulfate and SO₂ mixing ratios and wet deposition fluxes. Following *Kasibhatla et al. [1997]*, we calculated the percentages of comparison points whose model results were within a factor of 2 of the corresponding measurements for each parameter. The results are listed in Table 1. The domain averages for the comparison points were also calculated. As can be seen, about half of the observed sulfate mixing ratios were simulated to within a factor of 2, and the domain average of the modeled sulfate mixing ratios for the base run was 13% lower than the observation. Only ~25% of the sulfate wet deposition amounts were simulated to within a factor of 2, and the domain average of the model results was 76% higher than the observation for the base run. Although the modeled domain average of sulfate wet deposition for the “50%” case was close to the observations (25% overestimation) (Table 1), the “50%” case did not improve the model performance on the wet deposition spatially as shown in Figures 7d and 8. The model seriously overpredicted the sulfate wet deposition at most stations over the middle part of the domain (Figure 7c, d). Overprediction of sulfate wet deposition may be one of reasons leading to underprediction of sulfate mixing ratios over the Northeast (Figure 7a). The scatterplot of Figure 8 indicates that the model overpredicted sulfate wet deposition more when the observed sulfate wet deposition was less than 0.1 m mol m⁻² week⁻¹. Inspection of Figures 7 and 8 shows that most of locations where ratios of modeled to observed mean wet deposition was larger than 3.0 in Figure 7c and 7d were locations of low sulfate deposition. As noted by *Benkovitz and Schwartz [1997]*, departure of modeled and observed values may not be attributed entirely to performance of the model because the observed values at a station are not necessarily representative of the grid cell as a whole and may be not suitable for evaluation of the model, which means to represent the mean values over the grid cell. In addition to the problem in the representativeness of the observations at a single location for the grid cell as a whole, the discrepancy between the modeled and observed wet deposition can be due to inaccuracy in the representation of locations and amounts of precipitation in the meteorological forecast model (here, MM5) that drives the chemical transport model and in the representation of wet removal

processes [Seaman, 2000]. Discrepancies between model and observations might be due also to errors in boundary conditions, especially near the western edge of the model domain. Nonetheless, these considerations suggest a need to improve the accuracy of wet processes in the model.

For the sensitivity study with the doubled condensation rate, the domain averages of the modeled SO_4^{2-} mixing ratios for the 40-day simulation period were about 15% lower than for the base case (Table 1), and sulfate wet deposition about 7% higher, resulting in decreased overall model skill compared with observations. These changes are attributed to a shift in sulfate mass loading from the nucleation mode to the accumulation mode (diameter 0.1 to 1.0 μm). Most of sulfate aerosols, both in ambient and in present model, are located in the accumulation mode, whereas sea salt, dust, etc., which are not included in the model, are in the coarse mode, which would contribute little to surface area. Evidently the surface area for condensation is already accurately represented by the modeled sulfate without inclusion of coarse mode aerosol. This may be the major reason why a doubling of the condensation rate to account for aerosol species other than sulfate results in a decrease in model performance. As the accumulation mode is more efficiently removed by wet deposition than the nucleation mode, shifting sulfate from the nucleation mode to the accumulation mode enhances the removal rate.

It was found that the model performs better on the mean results of the 40-day period than on individual measurements. For instance, ~60% of the observed mean sulfate mixing ratios and ~53% of observed mean wet sulfate deposition were simulated to within a factor of 2, higher than those of the individual measurements for the base case (Table 1). These results are in agreement with the study of *Dennis et al.* [1993], who found that the absolute difference between observations and model results decreased rapidly for successively longer averaging period because of temporal noise in the dataset. It also probably means that the location of the material is displaced because of inaccuracies in the wind field of the meteorological driver, which would tend to average out.

The model systematically overestimated the observed SO_2 mixing ratios, as shown in Figure 8. Only 22% of the observed SO_2 mixing ratios were simulated to within a factor of 2, and the modeled domain average was 138% higher than the observations (Table 1).

Preliminary evaluation results of EPA's Models-3 CMAQ also found that SO₂ predications were biased high by a factor of 2 [Mebust *et al.*, 2002; R. Dennis, personal communication, 2002]. The overpredictions of SO₂ were caused mainly by the nighttime overestimation of SO₂ on the basis of comparison of hourly measurements of SO₂ from AIRS in 1990 with the CMAQ results [R. Dennis, personal communication, 2002]. A possible reason is the model's coarse vertical resolution that cannot adequately resolve sharp nocturnal gradients near the surface [J. Pleim, personal communication, 2002]. The overestimation of nighttime SO₂ will not lead to substantial overestimation of gas-phase oxidation of SO₂ during nighttime but may lead to overestimation of aqueous phase oxidation. At the GSM during the SEAVS period, we also found that the average of the model results for SO₂ (2.23 ppb) was much higher than the mean observed SO₂ concentration (0.31 ppb) measured by the IMPROVE (filter sampler of the National Park Service (NPS)) and that (0.92 ppb) measured by the HEADS (using Harvard-EPA annular denuder system) during the SEAVS period [Andrews *et al.*, 2000]. Andrews *et al.* [2000] ascribed the systematically lower SO₂ value (0.31 ppb) measured by the IMPROVE to absorption of SO₂ by the 8-foot aluminum inlet tube used in the IMPROVE sampler. This result suggests that some systematically lower SO₂ values of measurement methods may also be one of the reasons that lead to low observed SO₂ values compared to the model. SO₂ mixing ratios are also overpredicted in several global models [Kasibhatla *et al.*, 1997; Barth *et al.*, 2000; Chin *et al.*, 2000]. The additional possible reasons for the overestimation of SO₂ mixing ratios have been suggested: (1) additional heterogeneous mechanisms for the oxidation of SO₂ in the boundary layer; (2) non-representative locations and elevations of surface observation sites. Most of SO₂ is released from stacks above local shallow inversion layers, with the observation stations located close to the surface below the inversions.

3.3.3. Comparisons of vertical profiles of mass and number concentrations and size distributions with measurements over Nashville, Tennessee

The comparisons of modeled and observed vertical profiles of sulfate mass concentrations and size parameters over the Tennessee provide an assessment for the ability of the model to represent vertical structure of aerosol properties. In this study, the

data of two periods (period 1: 14:00-18:00 (GMT) July 19, 1995 and period 2: 12:00-16:00 (GMT) July 20, 1995) from the SOS experiment over Nashville, Tennessee, are used to compare with the model results of the base case. In order to compare the modeled and observed vertical profiles, the observed and modeled size distribution data were grouped according to the altitudes and longitudes and latitudes of the observations, and corresponding layer heights and longitudes and latitudes of the model grid cells for each period. The corresponding mean aerosol properties and SO₂ mixing ratios were calculated for each layer for the each period over the whole study region.

Figures 11 and 12 show the modeled and observed vertical profiles of mean sulfate mixing ratios, number concentrations, r_e , r_m , r_n and SO₂ mixing ratios as a function of height (pressure) over Tennessee for the periods 1 and 2, respectively. For period 1, the model generally captured the vertical variation patterns of the observed sulfate and SO₂ mixing ratios, number concentration and r_n as shown in Figure 11, especially for the highest SO₂ mixing ratio in the plumes at around 910 hPa. For period 2, the model captures the vertical variation patterns of sulfate mixing ratios and r_n well but poorly for other parameters as shown in Figure 10. Specifically, The model underpredicted the sulfate mixing ratios at low layers and high layers for both periods (Figures 9b and 10b). The model overpredicted SO₂ mixing ratios at low model layers for both periods but did not capture the observed SO₂ peak at around 910 hPa for period 2 (Figure 10f). This is consistent with those in section 3.3.1 that the model underpredicts the sulfate a little but overpredicts SO₂ by a factor of 2 at the ground layer.

Figures 9d and 10d indicate that the modeled mass mean radii are systematically smaller than the corresponding observations for both periods. As the observed aerosol size distributions are available between 0.05 and 1.75 μm particle radius in 15 size-bins measured by PCASP, we compared the mean observed size distributions with the surrogates to the size distributions retrieved by the RMST [Yue *et al.*, 1997; Wright *et al.*, 2002] on the basis of the corresponding mean six moments from the model. Figure 11 shows the examples of the comparisons of mean observed and modeled size distributions at the layers 2 (982 hPa), 7 (943 hPa) and 12 (822 hPa) for the two periods. In most cases the model has successfully captured the observed size distributions in the middle 6 bins of accumulation mode (e.g. bins with radius boundaries of 0.10, 0.125, 0.15, 0.20, 0.25,

0.35, and 0.45 μm) which were determined mainly by sulfate aerosol. This result is in agreement with the previous results obtained at the GSM (Figure 7). This is in agreement with the recent finding of *Brock et al.* [2002] over Nashville during the SOS' 99 field mission that sulfate contributed most of the mass of aerosol particles in the plumes from coal-fired power generation stations over Nashville on the basis of measurements of submicrometer particle size distributions in the plumes and the calculations of a numerical plume photochemistry model. *Husar et al.* [1978] also showed that sulfate was predominant composition of aerosol particles formed in power plant plumes. Figure 11 shows that the retrieved number concentrations at the radii larger than 0.50 μm are systematically lower than the observations for all layers like those at the GSM. However, the model does not underpredict the observed particles in the small size range like those at the GSM. For the SOS Nashville/Tennessee Field Intensive, one of its major goals was to examine the role of power plant plumes in oxidation formation and the interaction of these plumes with the Nashville urban plume [*Hubler et al.*, 1998; *McNider et al.*, 1998]. The power plant plumes can be identified by increased SO_2 concentrations whereas the urban plume can be detected by elevated CO concentration [*Brock et al.*, 2002]. The very high mean SO_2 concentrations at height of ~ 900 mb in both Figures 9f and 11f indicate that both periods were strongly influenced by the power plant plumes. This means that on the contrary to the observations at the GSM, the air masses in these two periods over Nashville contained substantial portions of material directly emitted by the power plants. Therefore, it is not surprising that the observed aerosol size distributions contained some large particles (radius $> 0.5 \mu\text{m}$) that may be not sulfate in the two periods as shown in Figure 11. This can explain the systematic underprediction of mass mean radius (Figures 9d and 10d) because the large particles other than sulfate in observations can make a substantial contribution to mass mean radius. This may be the reason that *Von Salzen et al.* [2000] also found their modeled mean mass radii based on the sulfate smaller than the observations over the Tennessee as well.

4. Spatial distributions of microphysical properties of aerosols over the eastern US during summer

One of major goals of this model is to simulate aerosol microphysical properties over the eastern US. Since our results were based only on the 40-day simulation from July 19 to August 28, 1995 and there was a Hurricane Erin even during the period, it needs to consider these extreme meteorological conditions when compared to other model's results. Figure 12 shows the horizontal spatial distributions of the 40-day mean sulfate mixing ratios and number concentrations at the lowest model layer over the eastern US for the base case. As can be seen, the high sulfate mixing ratios are located around the Ohio River valley, whereas the high number concentrations are located over the Northeastern Coast (New Jersey area) as well as the Ohio River valley. This is generally in agreement with the observations of eastern US $PM_{2.5}$ and PM_{10} patterns [EPA, 1996], in which the summer peaks ($\sim 40 \text{ g m}^{-3}$ for PM_{10} and $\sim 24 \text{ g m}^{-3}$ for $PM_{2.5}$) were determined over the Ohio River valley where sulfate is a major component of PM. As mass mean radii are available over eastern US in the modeling study of *von Salzen et al.* [2000], it is of interest to compare our results with theirs, although a direct comparison of the results of the two studies might not be appropriate because of different years (July 17-30, 1995 in this study vs July 17 to 30, 1994 in *von Salzen et al.* [2000]). The mass mean radius at ambient relative humidity in the present simulation is 0.15 ± 0.013 (one standard deviation) μm , fairly close to but somewhat higher than the mean value obtained by *von Salzen et al.* [2000] ($0.11 \pm 0.030 \text{ }\mu\text{m}$) for the corresponding cells over the eastern US. Examination of the spatial distributions of mass mean radius from the two models did not show evidence of strong spatial correlation. The reasons for this are not known—differences in emissions, model, or controlling meteorology.

To better understand the sources and vertical profiles of sulfate properties, we analyzed the sulfate aerosol properties and carried out process analysis at three specific locations over New Jersey, Ohio River valley and Atlantic Ocean shown in Figure 12a. Figure 13 shows the vertical profiles of mean number concentrations, sulfate, SO_2 and H_2SO_4 mixing ratios and mass mean radii for the three locations. As expected, both mean sulfate mixing ratios and number concentrations over the Ohio River valley were much higher than those over other two locations below layer 11 ($\sim 1.4 \text{ km}$). Somewhat

surprisingly, sulfate mixing ratios over the Atlantic Ocean location were greater than those over the New Jersey below layer 6 (~340 m) whereas the number concentrations over the Atlantic Ocean location were lower at the low model layers. This is consistent with the larger mass mean radii over the Atlantic Ocean location (Figure 13). As expected, both SO₂ and H₂SO₄ vertical profiles were the lowest over the Atlantic Ocean location. Because the number of layers used for emissions was limited to 14 (~2600 m) in the model, the mean number concentrations, sulfate, SO₂ and H₂SO₄ mixing ratios and mass mean radii were very close for the three locations above layer 15 (Figure 13).

To better understand the contribution of each process to formation of sulfate aerosol, we analyzed the column sulfate amount and number changes and their budget over the three locations for the 40-day simulation (Table 2). 77% of total sulfate was located below layer 14 (~2.6 km) over both New Jersey and Ohio River valley locations whereas only 56% sulfate was located below layer 14 for the Atlantic Ocean location. Aqueous phase reaction of SO₂ is the dominant sulfate source, contributing 70% over both New Jersey and Ohio River valley locations. This is close to those of *Roelofs et al.* [2001], who found on the basis of the simulations of 11 global sulfur cycle models that the contributions of aqueous phase oxidation of SO₂ were 59-67% for eastern North America. Over the Atlantic Ocean location, the aqueous reaction of SO₂ even contributed 82% of total sulfate source because of no emission there. The contributions of gas-phase reaction through condensation and nucleation to sulfate amount range from 18% over both Atlantic Ocean and Ohio River valley locations to 17% over New Jersey location. Wet deposition was a major sink over the three regions (Table 2). The wet deposition was a major sink over the southern Atlantic Ocean (~98%), whereas it only contributed to 24% and 33% of total sink over the New Jersey and Ohio River valley respectively. These results indicate that the contribution of each process to the sulfate mass fluxes can vary greatly from one area to another area. The sulfate mass column amounts (Table 2) were substantially higher than those of *Kasibhatla et al.* [1997] (~0.156 mmol m⁻²) and *Roelofs et al.* [2001] (0.133 mmol m⁻²) on the basis of the global CTM simulations for eastern North America in summer. However, as our results were for only 40-day period, these results may be not comparable.

In contrast to the sulfate amount, the percentages of total number of particles located below layer 14 (~2.6 km) were 59%, 48%, and 14% over Ohio River valley, New Jersey, and Atlantic Ocean locations respectively. The major portion of sulfate mass was located below 2.6 km whereas most of particle number was above 2.6 km except over Ohio River valley location (Table 2). This is reasonable because the large particles with major mass will exist at the low layers of the atmosphere and small particles with big contribution to total number concentration will exist at the high layers of the atmosphere. As analyzed by *Adams and Seinfeld* [2002], this vertical profile resulted from the higher nucleation rate in the upper troposphere and tropopause region and was in agreement with the observations of *Schroder et al.* [2002]. Over Ohio River valley, substantial portion of number budget was located below 2.6 km (layer 14) because major emissions occurred below 2.6 km over the area, and direct emissions were dominant sources of sulfate number concentration as analyzed below. Direct emissions were the dominant sources of particle number over both the New Jersey (99%) and Ohio River valley (96%) locations, whereas nucleation was only source of particle number at the Atlantic Ocean locations as listed in Table 2. As expected, coagulation was the dominant sink of particle number for all locations. Note, at the Ohio River valley and New Jersey locations total production of both sulfate amount and number substantially exceeds removal, whereas at the Atlanta Ocean location total removal exceeds production (Table 2). This indicates that the transport moved out substantial portion of the sulfate mass and number from the Ohio River valley and New Jersey locations, but that there was net import of sulfate mass and number into the Atlantic Ocean location. This is due to the fact that there was substantial emission at the Ohio River valley and New Jersey locations, as well as substantial sulfate formation by reaction, whereas at the Atlantic Ocean location there was no emission and much less reaction.

The lifetime of sulfate number is much shorter than sulfate amount because of the strong removal process of coagulation for the sulfate number (Table 2). For the three studied locations, the lifetimes of both sulfate amount and number over the Atlantic Ocean location (8.05 days for amount and 1.70 days for number) were much longer than those over the New Jersey location (4.97 days for amount and 0.38 days for number) and Ohio River valley location (2.56 days for mass and 0.17 days for number). The smaller

wet removal and coagulation rates over the Atlantic Ocean location lead to longer lifetimes for sulfate amount and number respectively as shown in Table 2. The longer lifetime of sulfate amount and number over the Atlantic Ocean may be another reason for the particles to become bigger than other locations (Figure 13). In the results of *Roelofs et al.* [2001], *Kasibhatla et al.* [1997] and *Chin et al.* [2000], the lifetimes of sulfate amount were 2.0 to 5.4, 2.7 and 3.4 days for eastern North America respectively. Our results seem consistent with these results, especially over the New Jersey and Ohio River valley.

5. Summary and Conclusions

A six-moment aerosol microphysical module (6M) has been implemented in a regional 3-D air quality model (MAQSIP) and applied to sulfate aerosol in the eastern US for 40 day simulation of July to August 1995. The model successfully captured the observed size distribution in the accumulation mode (radius 0.1 to 0.5 μm), in which the sulfate is predominately located, on the basis of the size distributions retrieved from the modeled six moments at the GSM during the SEAVS. These results demonstrate the utility as well as the efficiency of moment-based models. A one-day simulation needs \sim 8 hours computer time at a single-processor Sun (ULTRA 60) station. However, the model did not predict some of the moments well, especially the higher moments and during the dust events. Over the eastern US, the domain average of modeled SO_4^{2-} mixing ratios was 13% lower than the observations, with about 50% of the observations simulated to within a factor of 2. One of reasons for this underestimation of sulfate mixing ratios is thought to be overprediction of sulfate wet deposition. Reduction of the fraction of sulfate taken into cloud water from 100% to 50% does not improve the model performance spatially over the eastern US. The model systematically overestimated the observed SO_2 mixing ratios, by a factor of 2.4 on average.

The sensitivity test with doubled condensation rate suggests that most of the aerosol surface area, determined mainly by the accumulation mode, is well represented by the modeled sulfate. This is supported by the results that the model reproduced the effective radii better than other size parameters. Over Nashville during the SOS, the model closely reproduced the observed size distributions between 0.10 and 0.45 μm (dry radius), and

the observed and modeled sulfate mass concentrations are close as well. However, the model seriously underpredicted the observed high moments of total aerosol size distributions at the GSM during the periods when the site was influenced by the dust or the air mass transported from the Ohio River valley. Comparison of the observed and retrieved size distributions on the basis of the modeled six moments indicates that the model underpredicts the observed large particles (radius > 0.5 μm , coarse mode) and small particles (radius < 0.1 μm , nucleation mode) at the GSM and underpredicts the observed large particles over Nashville as well. In-situ chemical analyses indicated that other aerosol components such as dust and organics might make a substantial contribution to the observed particles in these two size ranges. Errors in the representation of sulfate nucleation or primary sulfate emissions might also cause these discrepancies, especially for the nucleation mode.

On the basis of the simulation of sulfate aerosols, it was found that the highest sulfate mass concentrations were located around the Ohio River valley whereas the high number concentrations were located over the Northeastern Coast (New Jersey area) and Ohio River valley. On the basis of column integral change and burden analysis of sulfate amount and number over the three locations, it was found that the contribution of each process varied considerably from one location to another location. The major portion of sulfate mass was located below 2.6 km and most of sulfate number locates above 2.6 km except over Ohio River valley where there was a major low-level input from emissions.

There are uncertainties in both quantitatively describing the aerosol dynamics and microphysics and in other atmospheric processes such as advection and diffusion represented in the model. Uncertainties in nucleation processes and rates are major limiting factors in modeling particle number and thus the modeling of other aerosol properties, for which knowledge of aerosol number size distributions is required. In light of these uncertainties, the performance of our 6M moments-based module in the regional model can be considered to successfully represent aerosol evolution and properties. On the other hands, as shown in comparisons with observations over GSM and Nashville, Tennessee, accurate representation of properties of the whole aerosol obviously must include other important aerosol constituents such as dust and organics, especially for the eastern US.

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Appendix A: Calculations of weighting function for distributing the precipitation rates to each layer

As mixing ratios of water vapor (q_v), cloud water q_c (ice, q_i), rainwater q_r (snow, q_s) mixing ratios (g kg^{-1}) and meteorological parameters such as wind speed are generated by the MM5, the weighting function for calculating the precipitation rates at each resolved cloud layer can be based on this available information. The steps to get the weighting function according to the equation for rainwater mixing ratios in the MM5 (*Grell et al.*, 1994) are as follows:

Step 1: the rates at which is cloud water is converted into precipitation through autoconversion (P_{RC}) and accretion (P_{RA}) processes, and the evaporation of rain (P_{RE}) are determined as follows [*Grell et al.*, 1994]:

$$P_{RC} = k_1(q_c - q_{crit}) \quad (\text{A1})$$

$$P_{RA} = \frac{1}{4} \rho a q_c E N_0 \frac{(3+b)}{\mathbf{I}^{3+b}} \quad (\text{A2})$$

$$P_{RE} = \frac{2\rho N_0 (S-1)}{A+B} \left[\frac{f_1}{\mathbf{I}^2} + f_2 \left(\frac{a\mathbf{r}}{\mathbf{m}} \right)^{1/2} S_c^{1/3} \frac{(5/2+b/2)}{\mathbf{I}^{5/2+b/2}} \right] \quad (\text{A3})$$

$$\mathbf{I} = \left(\frac{\rho N_0 \mathbf{r}_w}{\rho q_r} \right)^{1/4}$$

$$A = \frac{L_w^2 \mathbf{r}}{K_a R_v T^2}$$

$$B = \frac{1}{q_{sw} \mathbf{c}}$$

$$S_c = \frac{\mathbf{m}}{\mathbf{r}\mathbf{c}}$$

where the parameters (N_0 , a , b) of Marshall-Palmer size distributions for rain are: $N_0 = 8 \times 10^6 \text{ m}^{-4}$, $a = 842 \text{ m}^{1-b} \text{ s}^{-1}$, $b = 0.8$, $f_1 = 0.78$, $f_2 = 0.32$. Γ is the gamma function and \mathbf{m} is the dynamic viscosity of air. \mathbf{c} is diffusivity of vapor in air ($\text{m}^2 \text{ s}^{-1}$). \mathbf{r} and \mathbf{r}_w are the densities of air and rain respectively. $q_{crit} = 0.5 \text{ g kg}^{-1}$ and $k_1 = 10^{-3} \text{ s}^{-1}$. E is the collection efficiency (1 for rain, 0.1 for snow). L_w is the latent heat of evaporation and K_a is the thermal conductivity of air. R_v is the gas constant for water vapor ($461.5 \text{ J kg}^{-1} \text{ K}^{-1}$) and T

is the temperature (K). q_{sw} is saturated vapor mixing ratio with respect to water and S is relative humidity.

Step 2: the advection term in the equation for rainwater mixing ratio is estimated on the basis of rainwater mixing ratios and wind speeds at two cells adjacent to the cell, e.g., for x direction,

$$\frac{(u(i)q_r(i))}{x} = \frac{u(i+1)q_r(i+1) - u(i-1)q_r(i-1)}{2x} \quad (\text{A4})$$

where u is wind speed for x-direction and x is grid distance of the cell.

Step 3: By ignoring the divergence and diffusion terms that are small in the equation for rainwater mixing ratio, we estimate the rainfall term in the equation for each cell on the basis of output of cloudwater mixing ratios and rainwater mixing ratios for each hour from MM5 as follows:

$$R_N = [(P_{RE} + P_{RC} + P_{RA}) * t - q_r \text{ advection} * t] \quad (\text{A5})$$

where t is the time interval for model output (1 hour).

As MM5 does not output the production terms in (A5), we would have to rerun the MM5 and force it to output the instantaneous values for these terms if we want to evaluate each term in (A5). This is beyond the scope of this paper. However, the MM5-output surface precipitation amount is computed using these production terms in the model. Therefore, we can compare the MM5-predicted surface precipitation to that estimated from (A5). We found that the correlation between them was very high (correlation coefficient was 0.8880 for 35 day data (number of point is 5328)) for our studied region. This indicates that as a post processing tool, equation (A5) can be used to estimate the rain water flux at all layers. In this study, we use the estimated rainfall by (A5) as weighting functions to distribute the rainfall output from MM5 vertically to each layer.

Appendix B: In-cloud and below-cloud scavenging of SO₂, H₂SO₄ and sulfate aerosols

In this study both rainout (in-cloud scavenging) and washout (below-cloud scavenging) are treated as first-order loss and simultaneous processes without operator splitting. The first-order loss rate constant (K_R) for rainout is

$$K_R = \frac{R_r / (z)}{W_c} \quad (\text{B1})$$

where R_r is the precipitation rate for the whole cell ($\text{kg m}^{-2} \text{s}^{-1}$), D is the layer thickness (m), W_c is a liquid water content of cloud for the whole cell (kg m^{-3}). For washout the rate constant (K_w) is

$$K_w = (r)R_a / f_c \quad (\text{B2})$$

where (r) is a washout coefficient (mm^{-1}) normalized to the precipitation rate [Dana and Hales, 1976] and f_c is the cloud cover fraction for the cell. (r) is assumed to be 0.1 mm^{-1} for gaseous species. For aerosols, (r) depending on retrieved r_g and \mathbf{s}_g was computed on the basis of calculations of Dana and Hales [1976] for mass washout coefficients (Figure 2 of Dana and Hales [1976]) with the 4th-order polynomial equation. The lognormal parameters N , r_g and \mathbf{s}_g are obtained algebraically from any three of the six moments: \mathbf{m}_0 , \mathbf{m}_1 , and \mathbf{m}_2 are used here. R_a is the total precipitation rate integrated over all model layers above the whole cell currently treated (mm s^{-1}).

SO_2 is partitioned according to Henry's Law between the gas-phase, the cloud water, and the rain water from above that will pass through the cell during the time step. First, we partition the SO_2 between the gas-phase and the "total aqueous phase" consisting of the cloud water in the present cell plus the rainwater passing through the cell from all layers above the cell. The fraction of SO_2 in the aqueous phase is

$$F_{aq} = \frac{K_H (W_c + W_r)RT / \rho_{H_2O}}{1 + K_H (W_c + W_r)RT / \rho_{H_2O}} \quad (\text{B3})$$

where K_H is the Henry's Law constant for SO_2 (M atm^{-1}), and R is the ideal gas law constant. T is the temperature (K). ρ_{H_2O} is the density of water = 1000 kg m^{-3} . The dependence of K_H on pH is considered with the method of Schwartz [1986] on the assumption that pH is 4.5. The rainwater (W_r , kg m^{-3}) is

$$W_r = \frac{R_a t}{z} \quad (\text{B4})$$

So the fraction of SO_2 in the cloud water (F_{cw}) is:

$$F_{cw} = \frac{K_H (W_c)RT / \rho_{H_2O}}{1 + K_H (W_c + W_r)RT / \rho_{H_2O}} \quad (\text{B5})$$

and the fraction of SO₂ in the rain water (F_{rw}) is:

$$F_{rw} = \frac{K_H (W_r) RT / \mathbf{r}_{H_2O}}{1 + K_H (W_c + W_r) RT / \mathbf{r}_{H_2O}} \quad (\text{B6})$$

The total SO₂ concentration at time t ($[SO_2]_{tot}(t)$) in the grid cell is partitioned as

$$\begin{aligned} [SO_2]_{cw}(t) &= F_{cw} [SO_2]_{tot}(t) \\ [SO_2]_{rw}(t) &= F_{rw} [SO_2]_{tot}(t) \\ [SO_2]_g(t) &= (1 - F_{cw} - F_{rw}) [SO_2]_{tot}(t) \end{aligned}$$

where cw , rw and g represents cloud water, rainwater and gaseous phase respectively.

These concentrations are then updated as follows:

For rainout we have

$$[SO_2]_{cw}(t + \Delta t) = [SO_2]_{cw}(t) \exp(-K_R \Delta t) \quad (\text{B7})$$

For washout the treatment depends on whether the process is limited by mass transfer

$$\begin{aligned} [SO_2]_{rw}(t + \Delta t) &= [SO_2]_{rw}(t) \exp(-K_w \Delta t) && \text{if } F_{rw} > 1 - \exp(-K_w \Delta t) \\ &&& \text{with } (r) = 0.1 \text{ mm}^{-1} \end{aligned}$$

or Henry's Law equilibrium:

$$\begin{aligned} [SO_2]_{rw}(t + \Delta t) &= [SO_2]_{rw}(t) (1 - F_{rw}) && \text{if } F_{rw} < 1 - \exp(-K_w \Delta t) \\ &&& \text{with } (r) = 0.1 \text{ mm}^{-1} \end{aligned} \quad (\text{B8})$$

The gas-phase portion remains unchanged by these processes as follows

$$[SO_2]_g(t + \Delta t) = [SO_2]_g(t)$$

The updated total SO₂ concentration in cloudy portion of the cell is

$$[SO_2]_{cld}(t + \Delta t) = [SO_2]_{cw}(t + \Delta t) + [SO_2]_{rw}(t + \Delta t) + [SO_2]_g(t + \Delta t)$$

If the cloud cover fraction (f_c) is less than unity, the updated mean SO₂ in the whole cell is

$$[SO_2](t + \Delta t) = f_c [SO_2]_{cld}(t + \Delta t) + (1 - f_c) [SO_2]_{clr}(t + \Delta t)$$

where the updated SO₂ concentration in clear-sky portion of the cell $[SO_2]_{clr}(t + \Delta t) = [SO_2](t)$ since at this point in the model integration clear-sky processes are not currently

being treated. H_2SO_4 is assumed to be completely in the aqueous phase, and partitioned between the cloudwater and rainwater according to their relative amounts:

$$[H_2SO_4]_{cw}(t) = [H_2SO_4](t) \frac{W_c}{W_c + W_r}$$

$$[H_2SO_4]_{rw}(t) = [H_2SO_4](t) \frac{W_r}{W_c + W_r}$$

and the updating is

$$[H_2SO_4]_{cw}(t + \Delta t) = [H_2SO_4]_{cw}(t) \exp(-K_r \Delta t)$$

$$[H_2SO_4]_{rw}(t + \Delta t) = [H_2SO_4]_{rw}(t) \exp(-K_w \Delta t)$$

and the updated total H_2SO_4 concentration in cloudy portion of the cell is

$$[H_2SO_4]_{cld}(t + \Delta t) = [H_2SO_4]_{cw}(t + \Delta t) + [H_2SO_4]_{rw}(t + \Delta t)$$

If the cloud cover fraction is less than unity, the updated mean H_2SO_4 in the whole cell is

$$[H_2SO_4](t + \Delta t) = f_c [H_2SO_4]_{cld}(t + \Delta t) + (1 - f_c) [H_2SO_4]_{clr}(t + \Delta t)$$

where $[H_2SO_4]_{clr}(t + \Delta t) = [H_2SO_4](t)$.

Sulfate aerosol is assumed to be completely in the aqueous phase, and partitioned between the cloudwater and rainwater according to their relative amounts. The number concentration of the aerosol (n_0) is partitioned as

$$[n_0]_{cw}(t) = [n_0](t) \frac{W_c}{W_c + W_r}$$

$$[n_0]_{rw}(t) = [n_0](t) \frac{W_r}{W_c + W_r}$$

and the updating is

$$[n_0]_{cw}(t + \Delta t) = [n_0]_{cw}(t) \exp(-K_r \Delta t)$$

$$[n_0]_{rw}(t + \Delta t) = [n_0]_{rw}(t) \exp(-K_w \Delta t)$$

and the updated mean aerosol number concentration in the cloud fraction of the cell is

$$[n_0]_{cld}(t + \Delta t) = [n_0]_{cw}(t + \Delta t) + [n_0]_{rw}(t + \Delta t)$$

If the cloud cover fraction is less than unity, the updated mean aerosol number concentration in the whole cell is

$$[n_0](t + \Delta t) = f_c [n_0]_{cld}(t + \Delta t) + (1 - f_c) [n_0]_{clr}(t + \Delta t)$$

As the removal must be done after completing the microphysical processes, we save the factor:

$$f_{fract} = \frac{[\mathbf{m}_0]_{cld}(t + \Delta t)}{[\mathbf{m}_0](t)}$$

to represents the fraction of the aerosol remaining after rainout and washout in the cloudy portion of cell. Note that this fraction of the aerosol was also applied to all six moments because the moments of a PDF are not mathematically independent quantities as analyzed in Section 2.2.

Figure Caption

Figure 1. The MAQSIP model domain and distribution of sulfur ($\text{SO}_2 + \text{SO}_4^{2-}$) emission over the eastern US in summer including both surface and elevated sources (See text). Unit is $\text{g m}^{-2} \text{ yr}^{-1}$.

Figure 2 (a) the time-series of the observed mass concentrations of $\text{PM}_{2.5}$ mass, sulfate, and inorganics ($\text{SO}_4^{2-} + \text{NO}_2^- + \text{NO}_3^- + \text{NH}_4^+ + \text{Na}^+ + \text{Cl}$); (b) organic carbon (OC), element carbon (EC), Cl and soil ($2.14 * \text{Si} + 2.89 * \text{Al} + \text{K} + \text{Ca} + \text{Fe} + \text{Mg}$) mass [Sherman *et al.*, 1997]; (c) the time-series of observed and modeled sulfate at the GSM during the SEAVS period.

Figure 3. Time-series of modeled and observed six moments at the Great Smoky Mountains. The observed six moments were calculated on the basis of measurements obtained by Kreidenweis *et al.* [S. Kreidenweis, R. Ames and J. Hand, private communication, 2002; Ames *et al.*, 2000]

Figure 4. Time-series of modeled and observed effective radius (r_e), mass mean radius (r_m), number mean radius (r_n) and standard deviation of radius at the GSM.

Figure 5. Comparisons of the observed and modeled size distributions at different times on the Great Smoky Mountains during SEAVS period. Note that the modeled size distributions were retrieved by the RMST method on the basis of the modeled moments (see text explanation).

Figure 6. Time-series of modeled and observed six moments at the Black Mountain in the summer of 1995.

Figure 7. Ratios of the modeled to the observed variables at individual grid box locations during the period July 19-August 28, 1995 over the eastern US. Those for mean sulfate mass concentrations were shown in (a) and (b) for “100%” and “50%” cases respectively. Those for mean wet sulfate deposition fluxes were shown in (c) and (d) for “100%” and “50%” cases respectively.

Figure 8. Comparisons of simulated and observed mean SO_2 and SO_4^{2-} mixing ratios and total wet deposition fluxes for the “100%” and “50%” model simulations for individual measurements during July 19-August 28, 1995 (40 days). The 1:1, 2:1 and 1:2 lines are shown for reference.

Figure 9. Vertical profiles of modeled and observed (a) number mixing ratios, (b) sulfate mixing ratios, (c) effective radii, (d) mass mean radii, (e) number mean radii and (f) SO_2 mixing ratios as a function of height (pressure) at Nashville, Tennessee during period 1 (14:00-18:00 (GMT) July 19, 1995). Note that 1 particle per mg of air corresponds to 0.78 particle per cm^3 at 1 bar and 273K.

Figure 10. The same as Figure 9 but for the period 2 (12:00-16:00 (GMT) July 20, 1995)

Figure 11. The same as Figure 5 but for layers 2 (~76 m), 7 (~480 m) and 12 (~1750 m) at Nashville, Tennessee, during period 1(14:00-18:00 July 19, 1995 ((a), (b) and (c))) and period 2 (12:00-16:00 July 20, 1995 ((d), (e) and (f))).

Figure 12. The 40-day average values of the horizontal distributions of (a) mean sulfate mixing ratios (μm , ppb) and (b) number (μ , cm^{-3}) concentrations at the lowest model layer. Circles at Ohio River valley, New Jersey, and the Atlantic Ocean east of Georgia in (a) denote the locations selected for budget analysis (see text explanation). The middle cells of the surrounding 9 cells (3x3) for each area are cell (60,50) (latitude: 39.41 N, longitude: -76.13 W), cell (40,46) (latitude: 38.87 N, longitude: -84.86 W) and cell (60,22) (latitude: 30.31 N, longitude: -77.94 W) for New Jersey area, Ohio River valley and Atlantic Ocean, respectively.

Figure 13. The mean vertical profiles of sulfate mass, SO_2 and H_2SO_4 mixing ratios, number concentrations, and mass mean radii over the three locations (New Jersey, Ohio River valley and Atlantic Ocean) during the 40-day simulation period. Height for each layer is also shown in the last panel.

Table 1. Statistical summaries of the comparisons of model results with observations over eastern US. $\langle C \rangle$: grand average, Percentages: are the percentages of the comparison points whose model results are within a factor of 2 of the measurements. Unit of wet deposition is $\text{m mol m}^{-2} \text{ week}^{-1}$. “50”, “100” and “OBS” represent the model results of “50%” and “100%” cases, and observations (see text)

Parameters	$\langle C \rangle$			Within factor of 2 (%)	
	100%	50%	OBS	100%	50%
SO ₂ , ppb	2.62	2.62	1.10	22	22
SO ₄ ²⁻ , ppb	1.63	1.83	1.87	46	56
*SO ₄ ²⁻ , ppb	1.40	1.61	1.87	45	46
Wet deposition	0.97	0.69	0.55	25	32
*Wet deposition	1.04	0.74	0.55	24	31

* For the cases with doubled condensation rate

Table 2. Column integral of change and column amount in sulfate amount and number concentrations by each process at three locations over New Jersey, Ohio Valley and Atlantic Ocean during the 40-day simulation period

	Ohio River valley	New Jersey	Atlantic Ocean
Column sulfate change (mmol m⁻² day⁻¹)			
Aqueous-phase reaction	0.56	0.33	0.028
Emission	0.15	0.059	0
Nucleation	2.12 10 ⁻⁵	0.45 10 ⁻⁵	0.19 10 ⁻⁵
Condensation	0.097	0.080	0.0055
<i>Total production</i>	<i>0.81</i>	<i>0.47</i>	<i>0.034</i>
Wet deposition	-0.26	-0.11	-0.04
Dry deposition	-9.32 10 ⁻⁴	-6.01 10 ⁻⁴	-6.19 10 ⁻⁴
<i>Total removal</i>	<i>-0.26</i>	<i>-0.11</i>	<i>-0.04</i>
Sulfate column burden (mmol m⁻²)			
Total	0.67	0.54	0.33
Below layer 14 (~2.6 km)	0.52	0.42	0.19
In layer 1 (~38 m)	1.12 10 ⁻²	0.46 10 ⁻²	0.49 10 ⁻²
Lifetime (day)	2.56	4.97	8.05
Column number change (10⁸ cm⁻² day⁻¹)			
Emission	136.0	55.1	0
Nucleation	6.15	0.79	0.19
<i>Total production</i>	<i>142.2</i>	<i>55.9</i>	<i>0.19</i>
Wet deposition	-3.9	-0.95	-0.62
Coagulation	-114	-42.7	-6.94
Dry deposition	-0.56	-1.0	-6.0 10 ⁻³
<i>Total removal</i>	<i>-118.4</i>	<i>-44.6</i>	<i>-7.56</i>
Number column burden (10⁸ cm⁻²)			
Total	20.3	17.1	12.9
Below layer 14 (~2.6 km)	11.9	8.18	1.74
In layer 1 (~38 m)	0.07	0.08	0.002
Lifetime (day)	0.17	0.38	1.70

*Note: Lifetime is defined as the ratio of column amount to the total loss rate excluding transport.

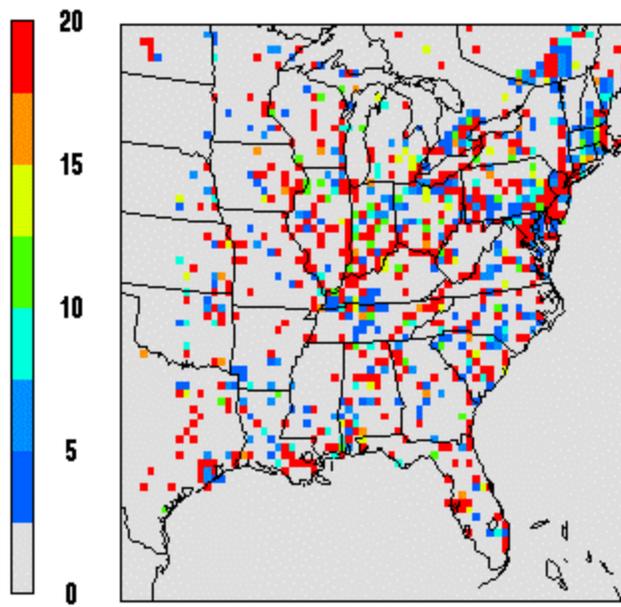


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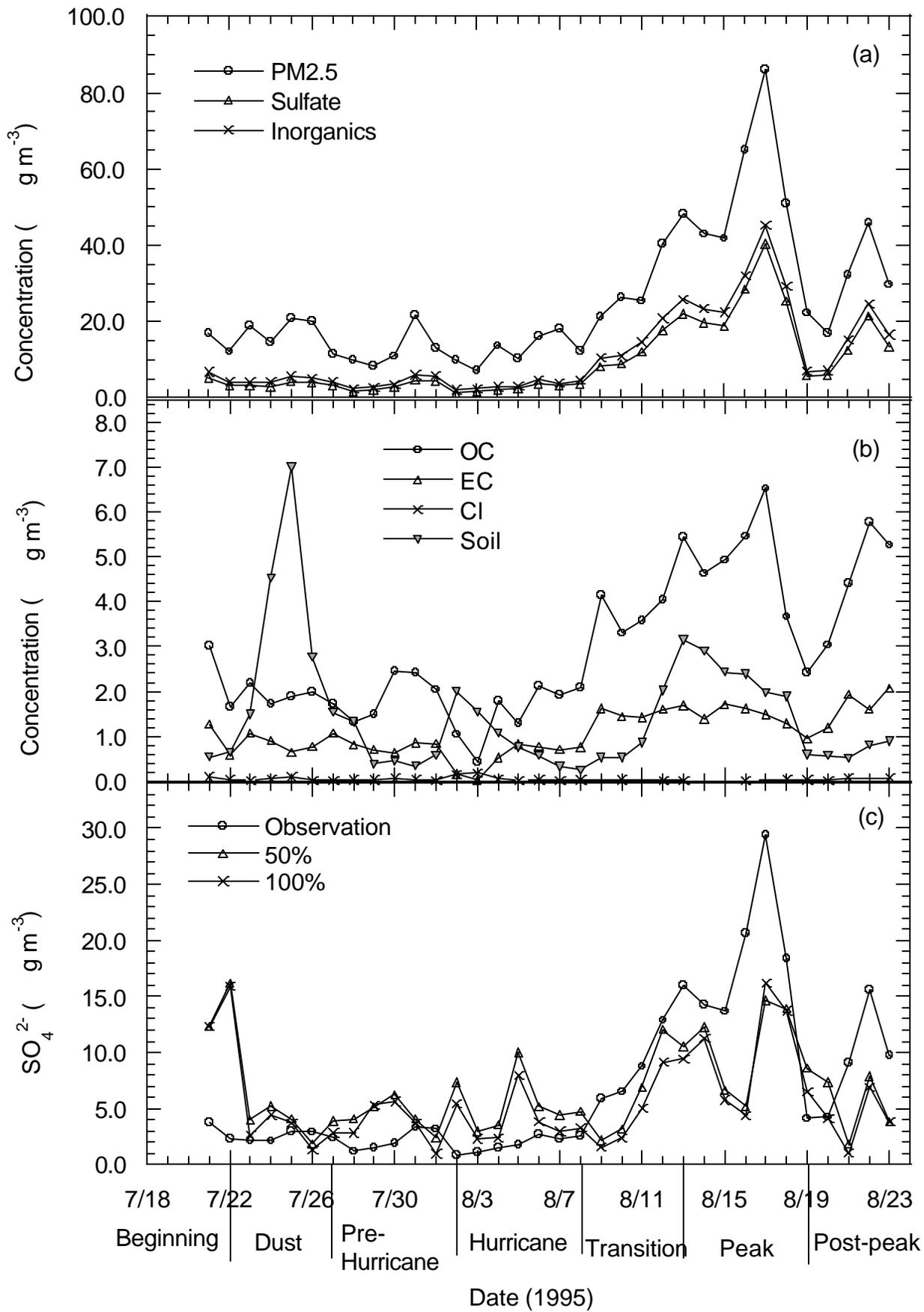


Figure 2

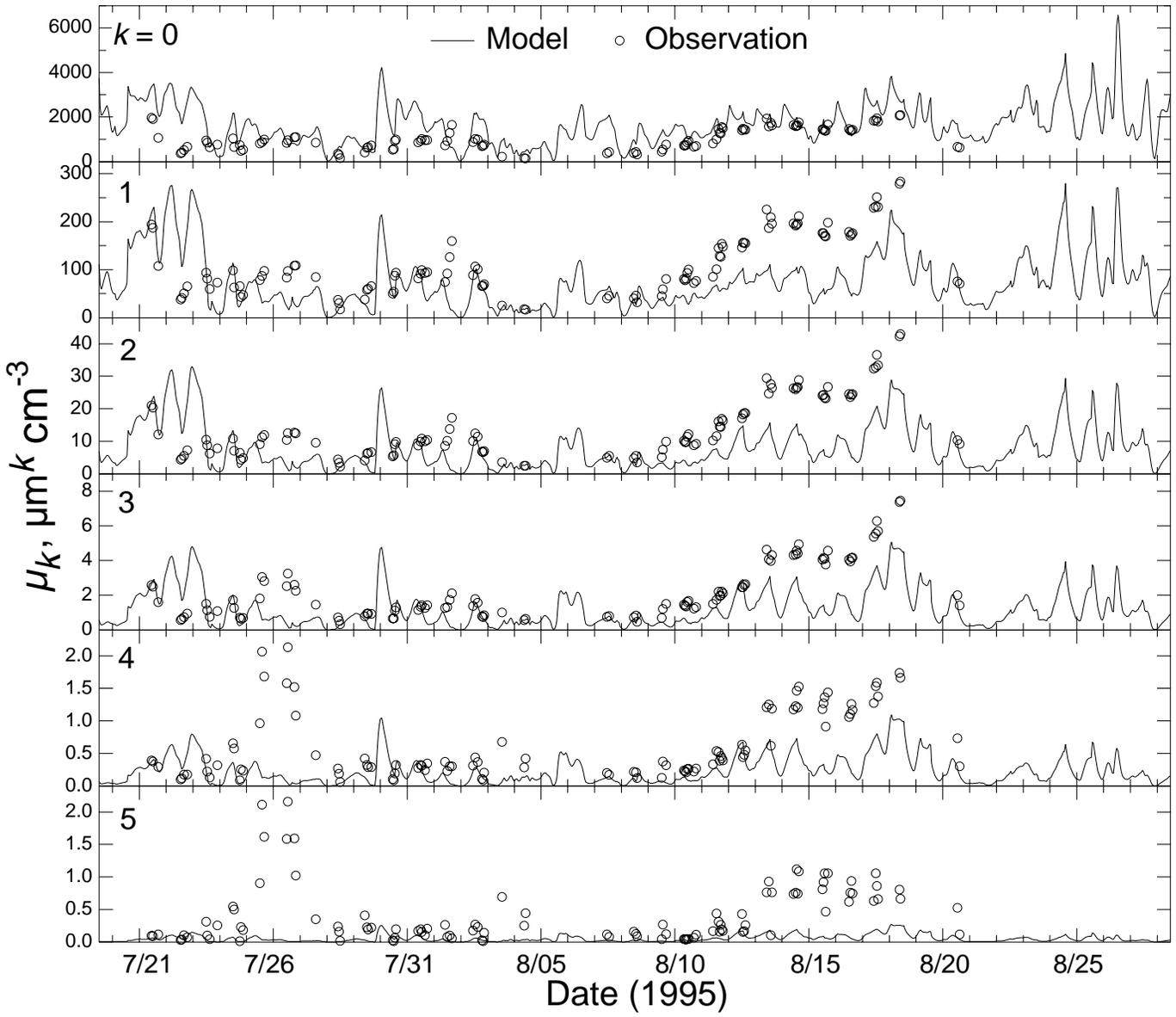


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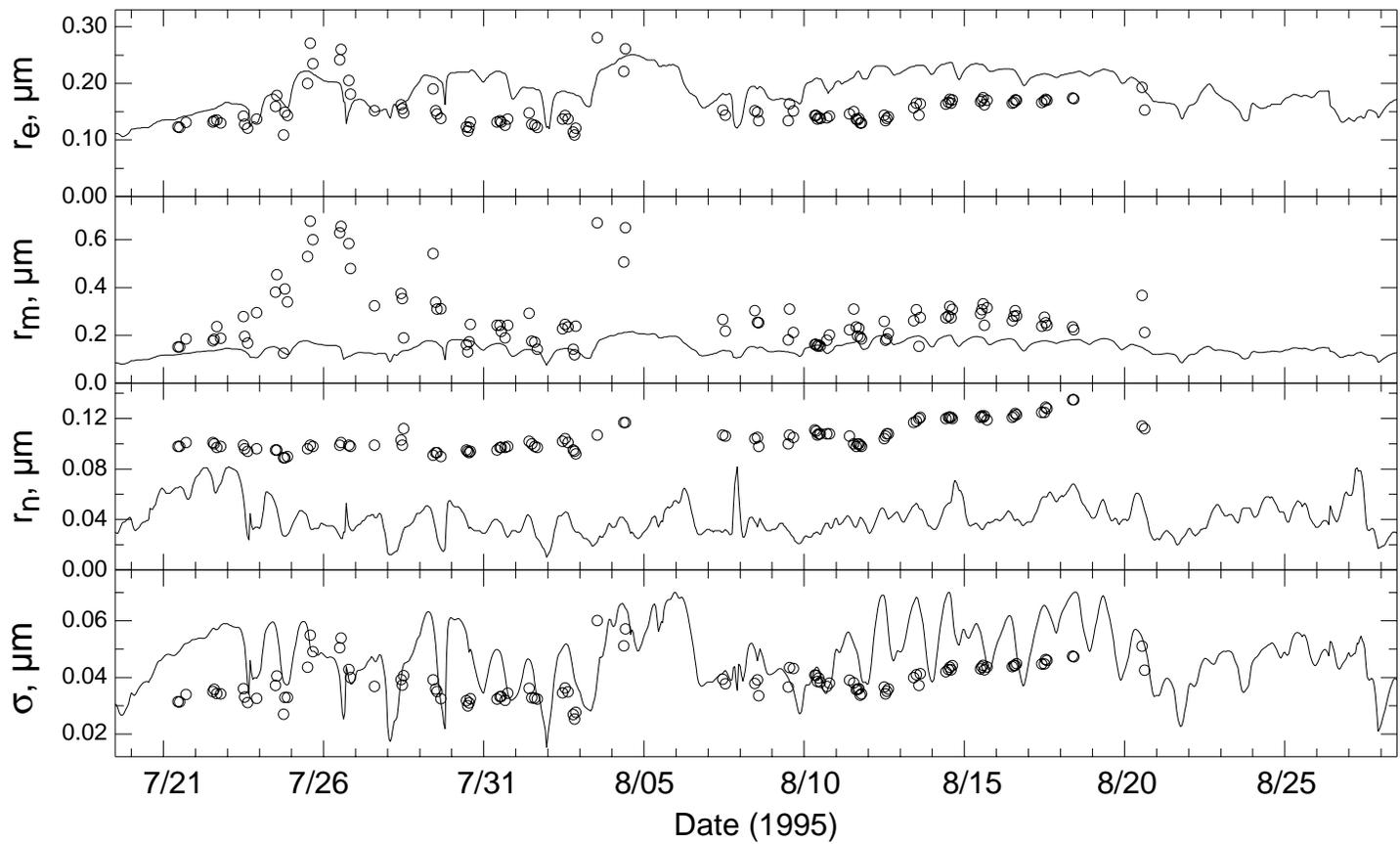


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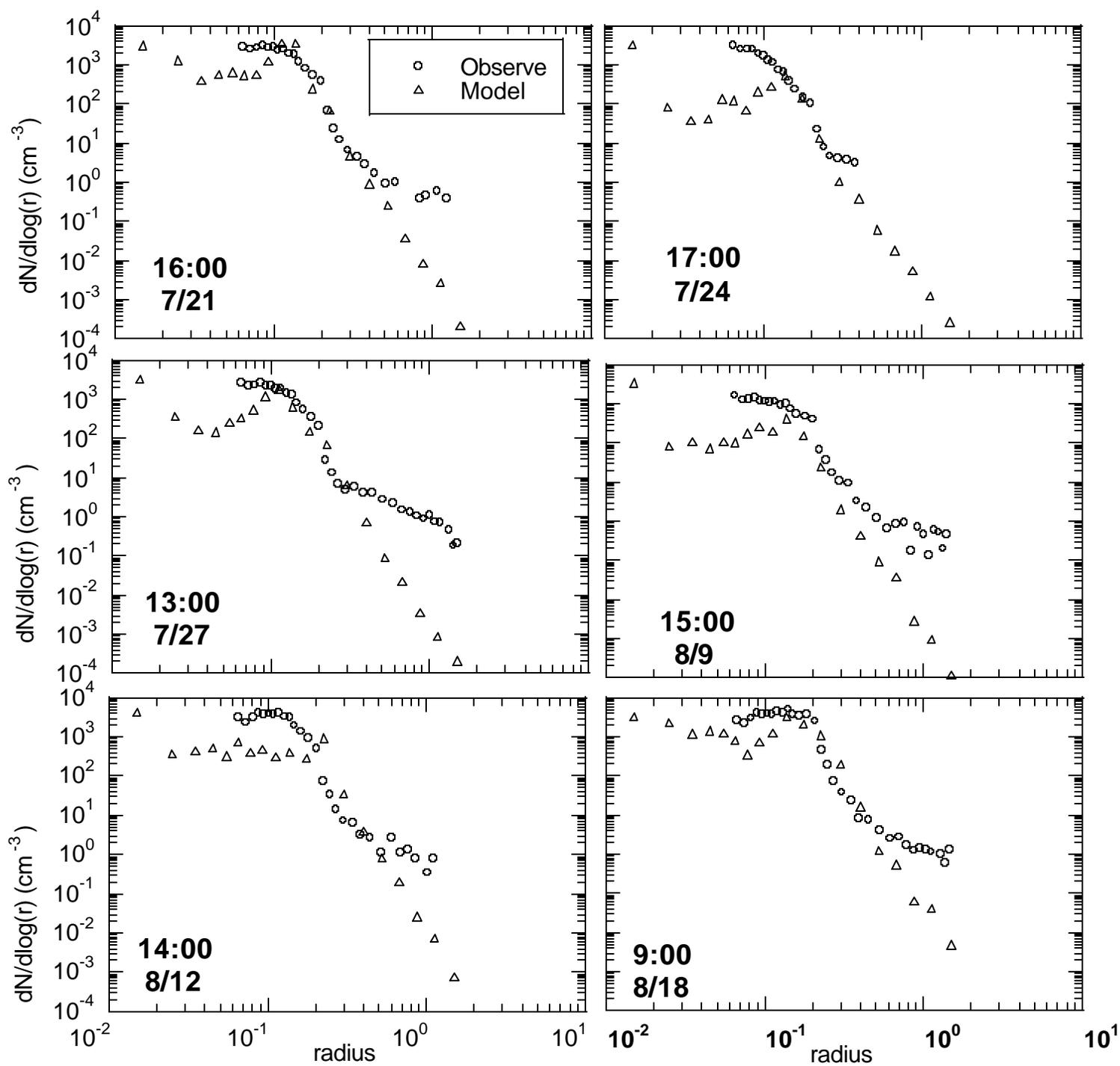


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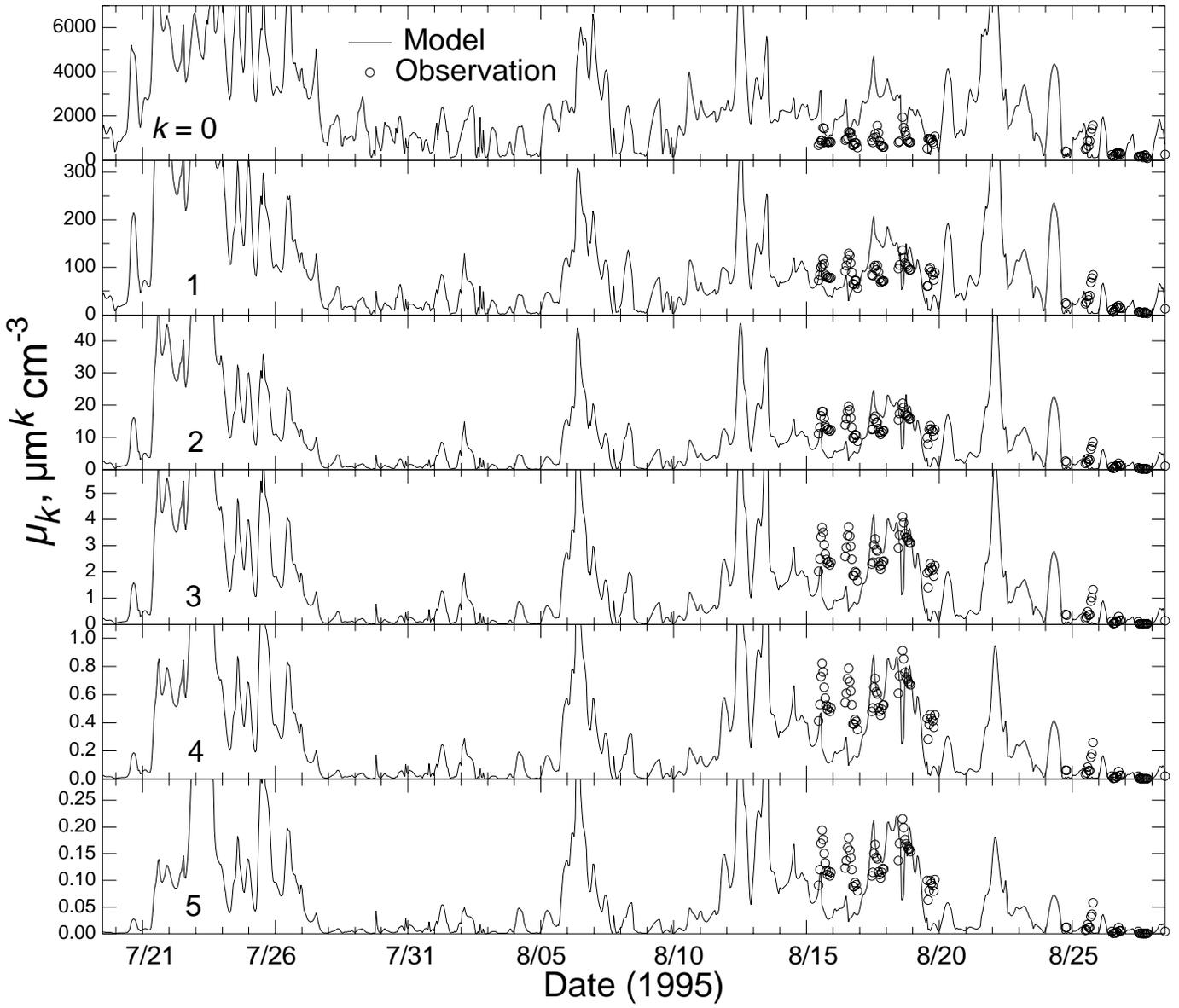
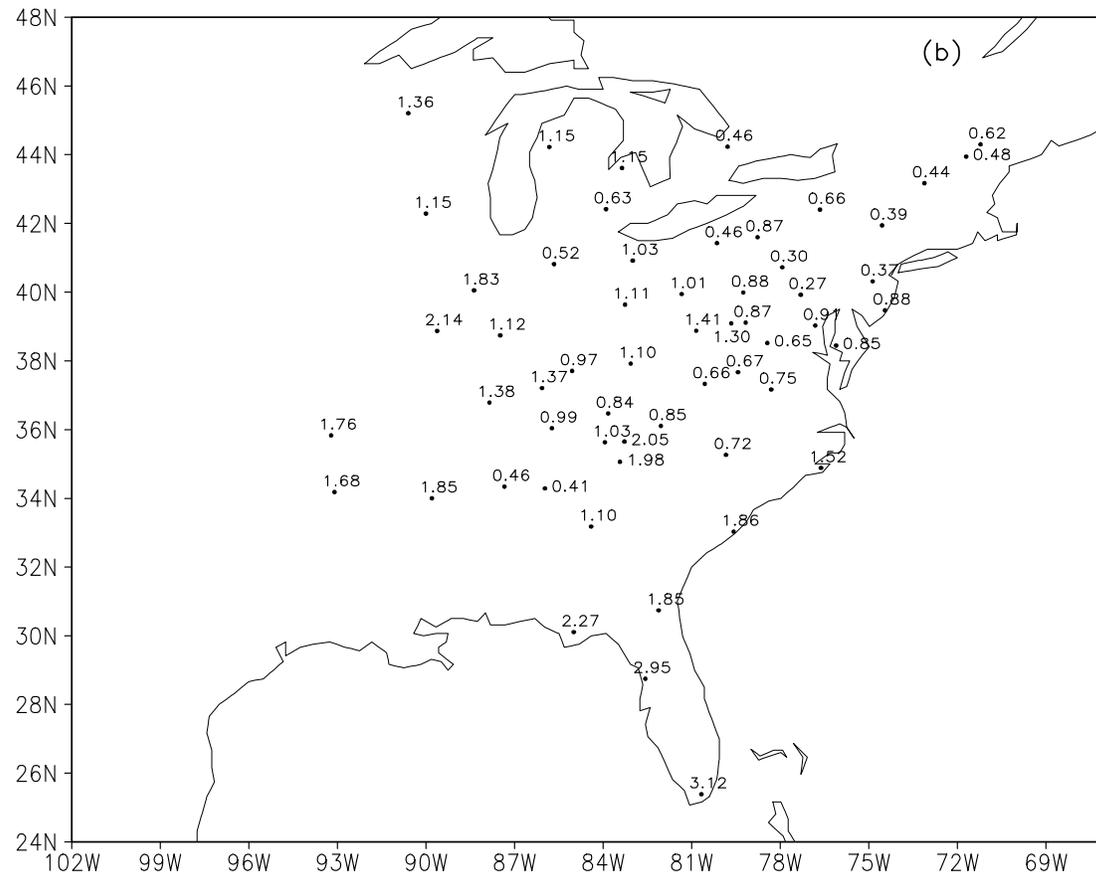
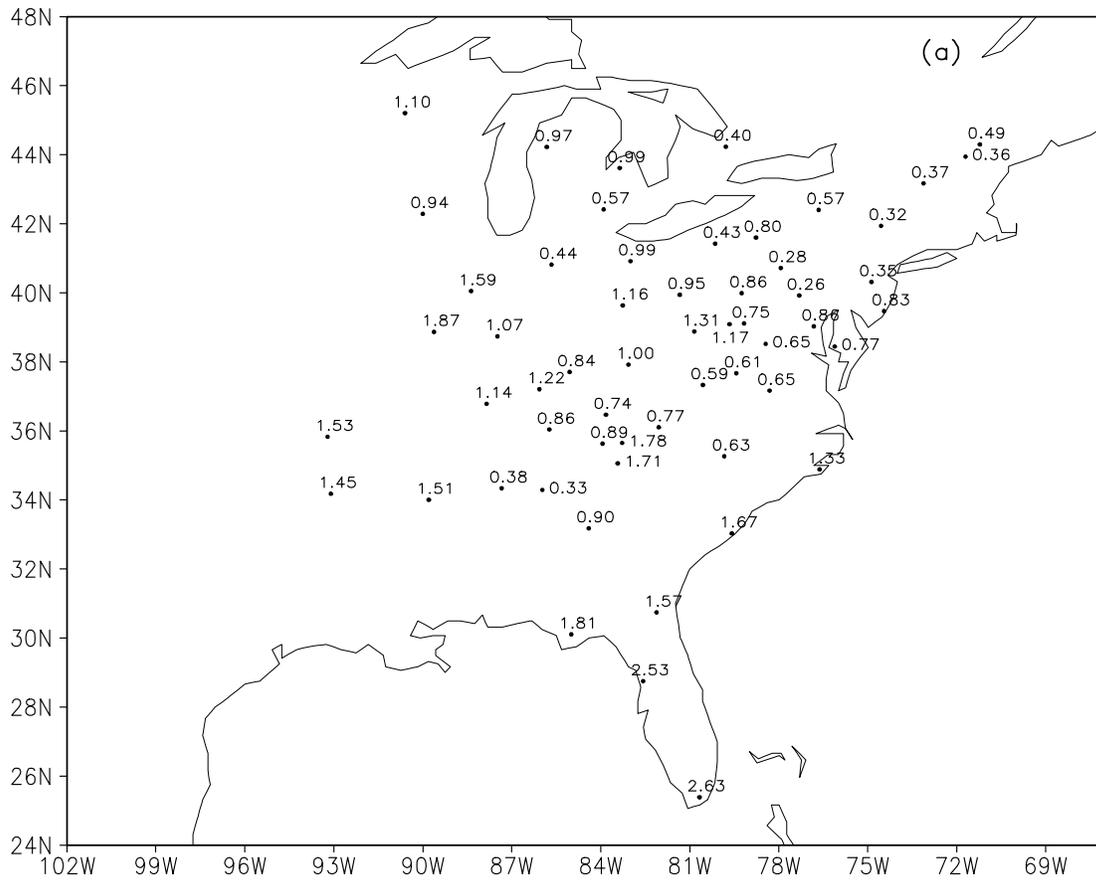


Figure 6



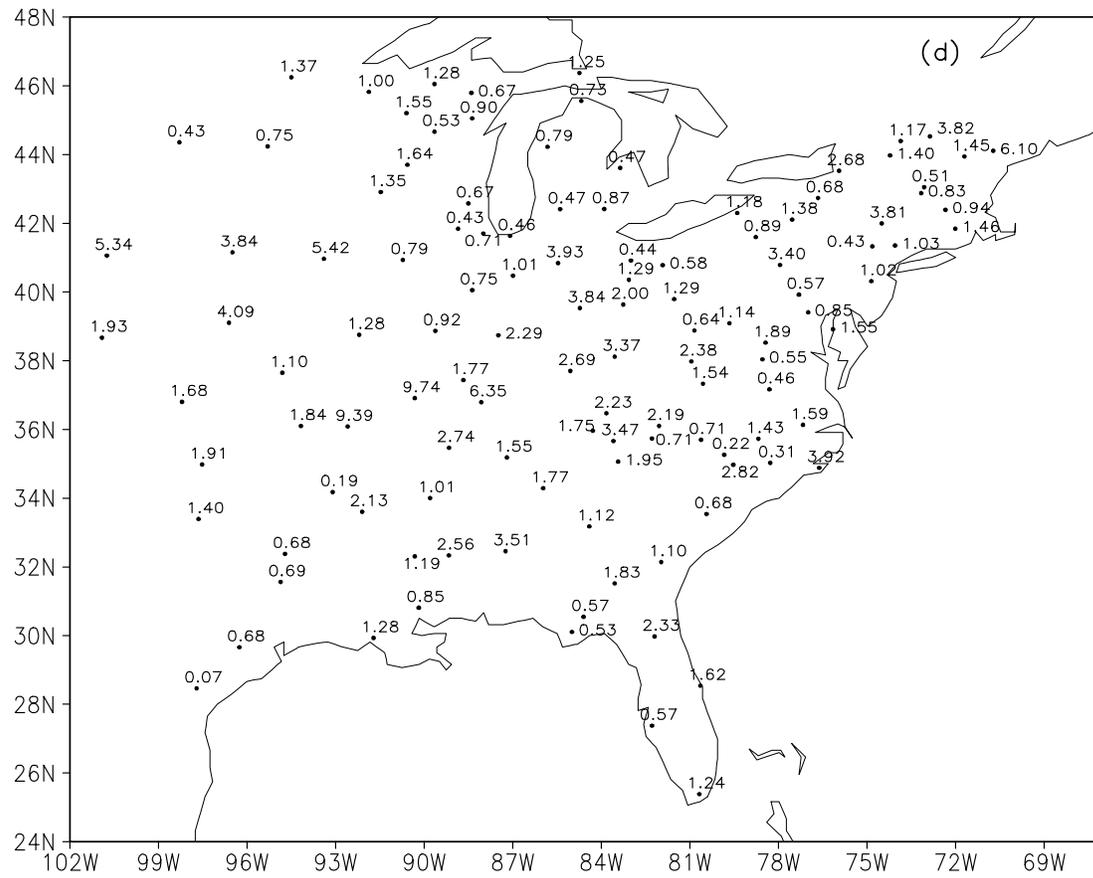
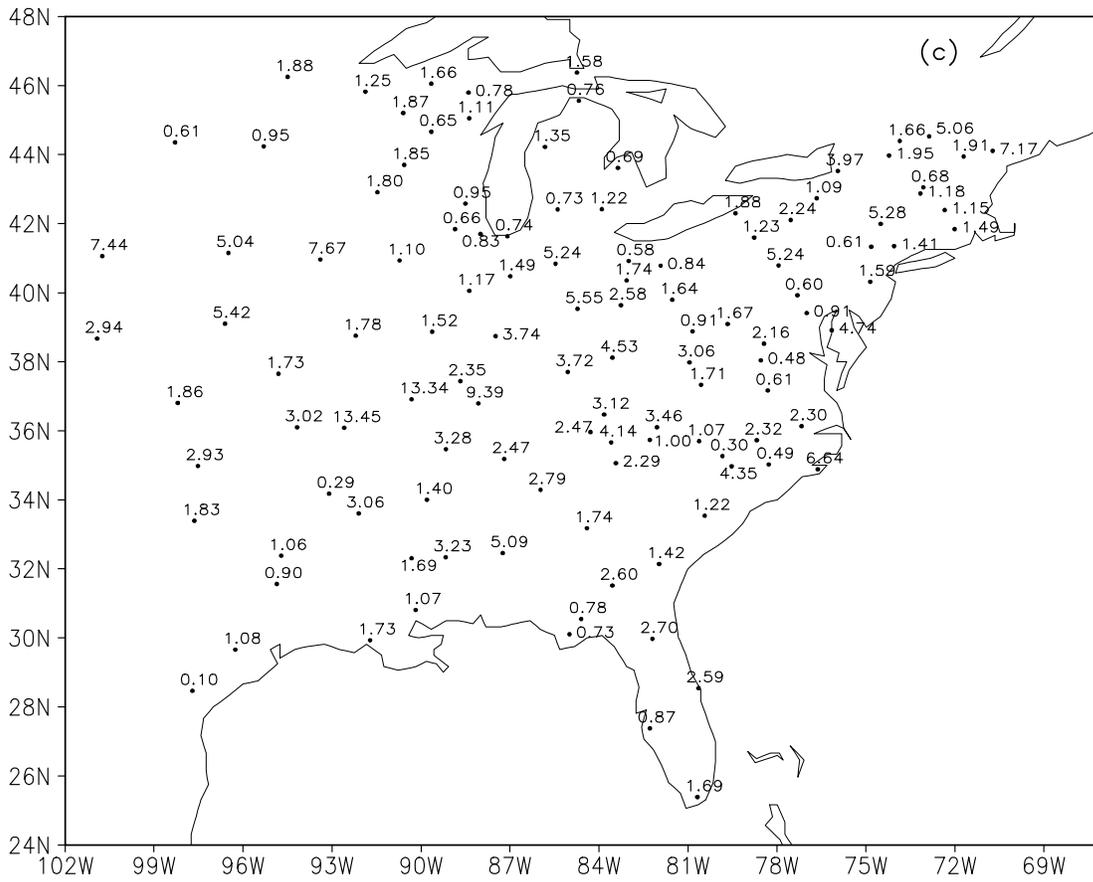


Figure 7 c, d

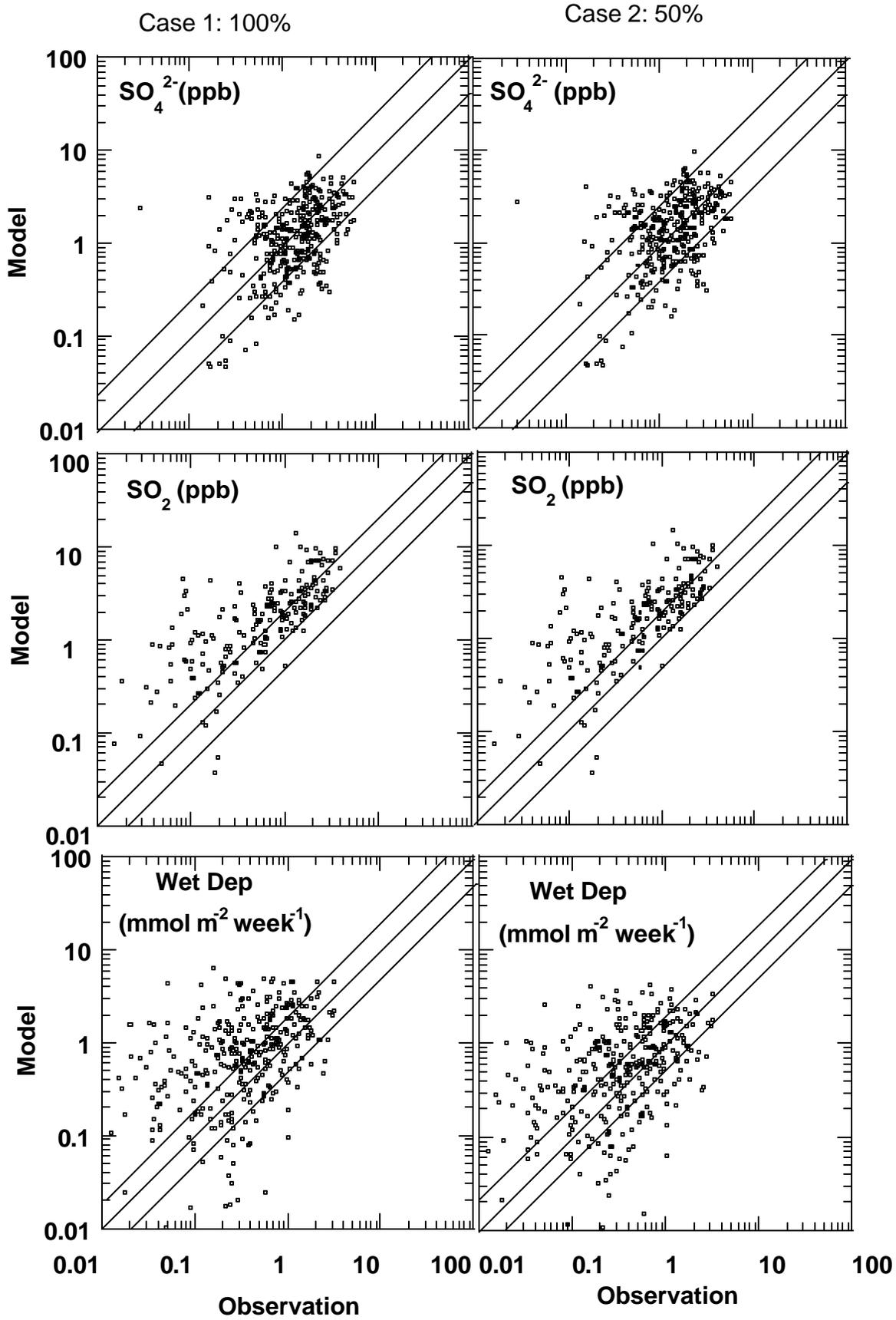


Figure 8

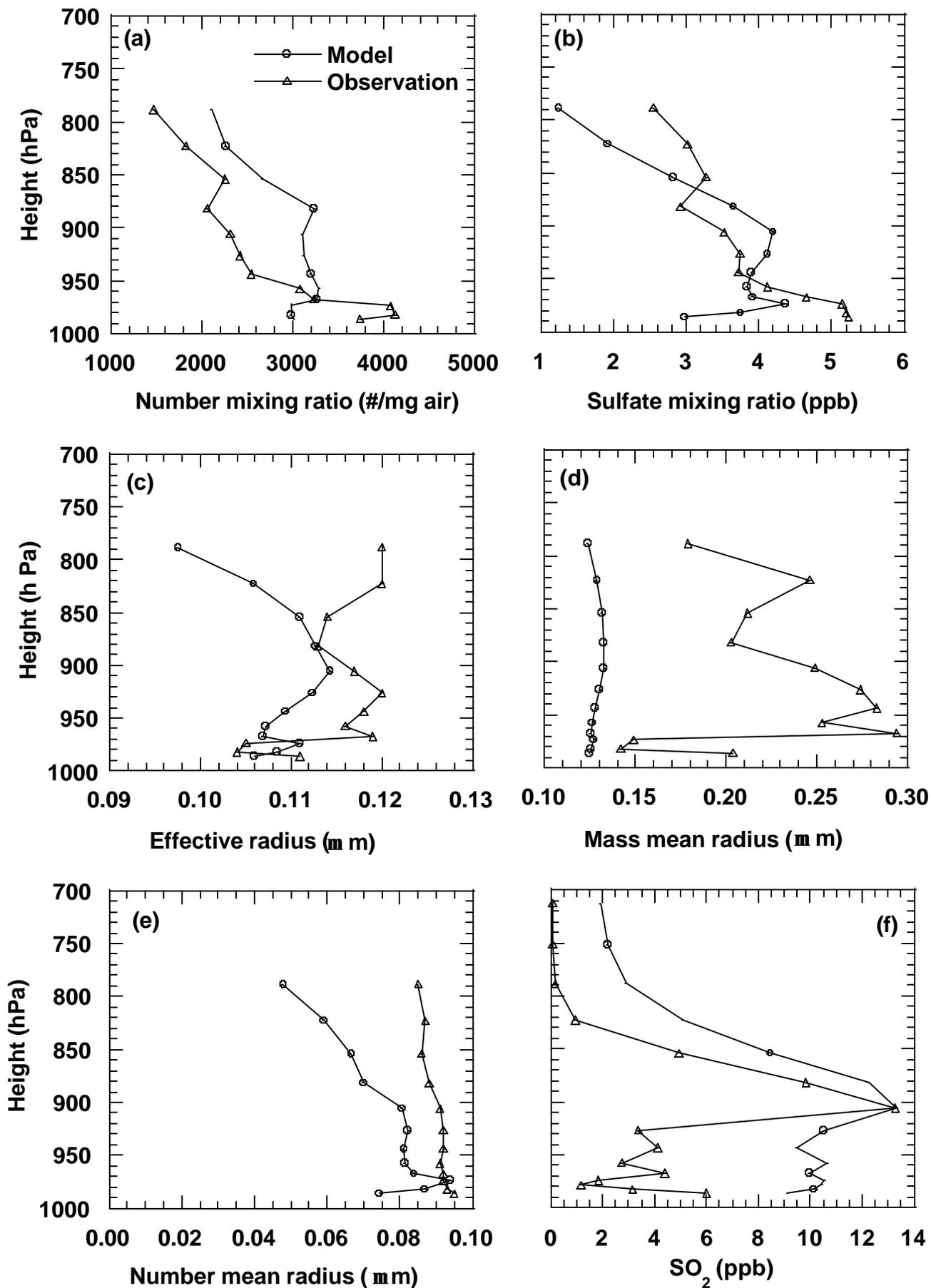


Figure 9

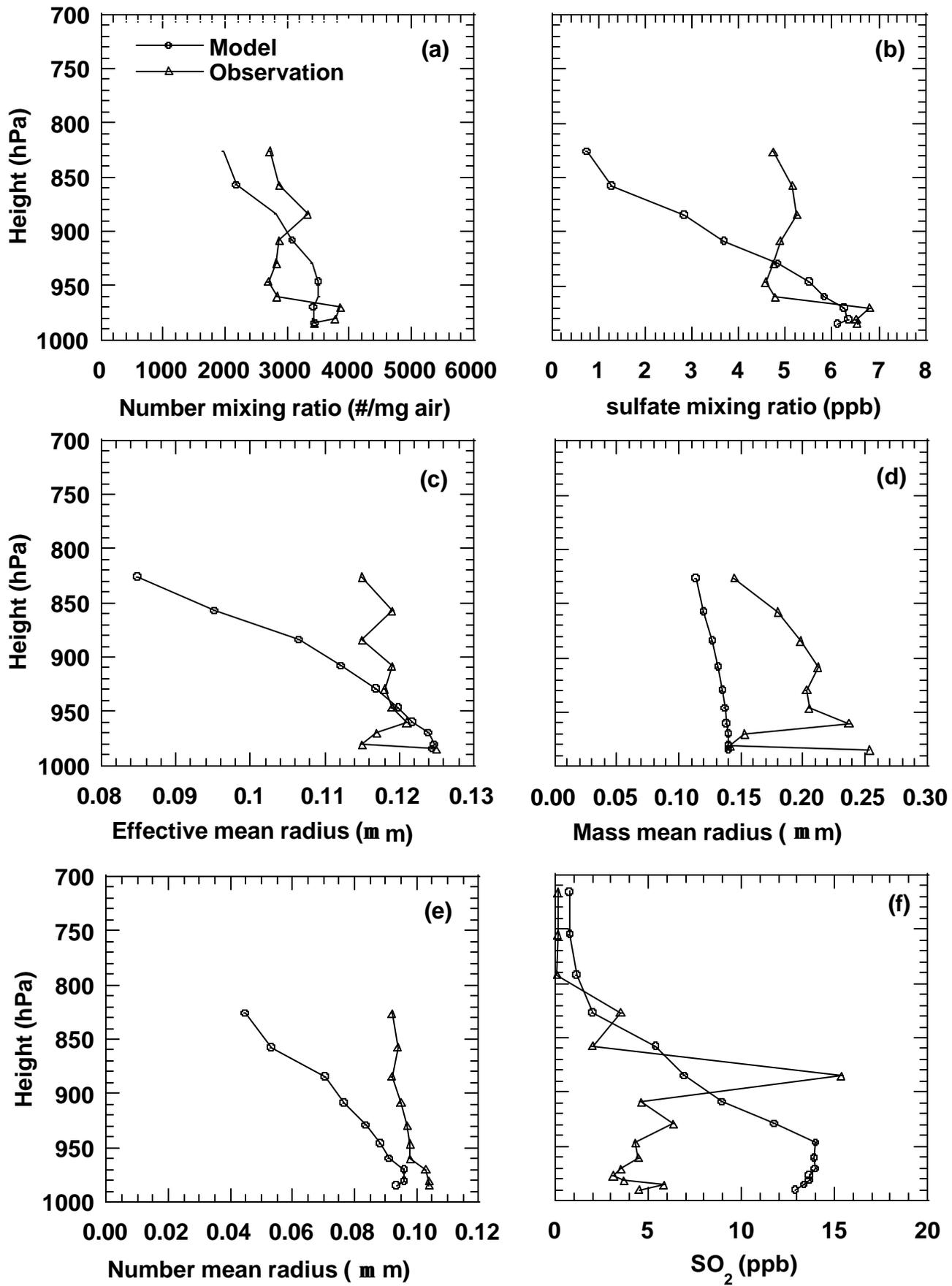


Figure 10

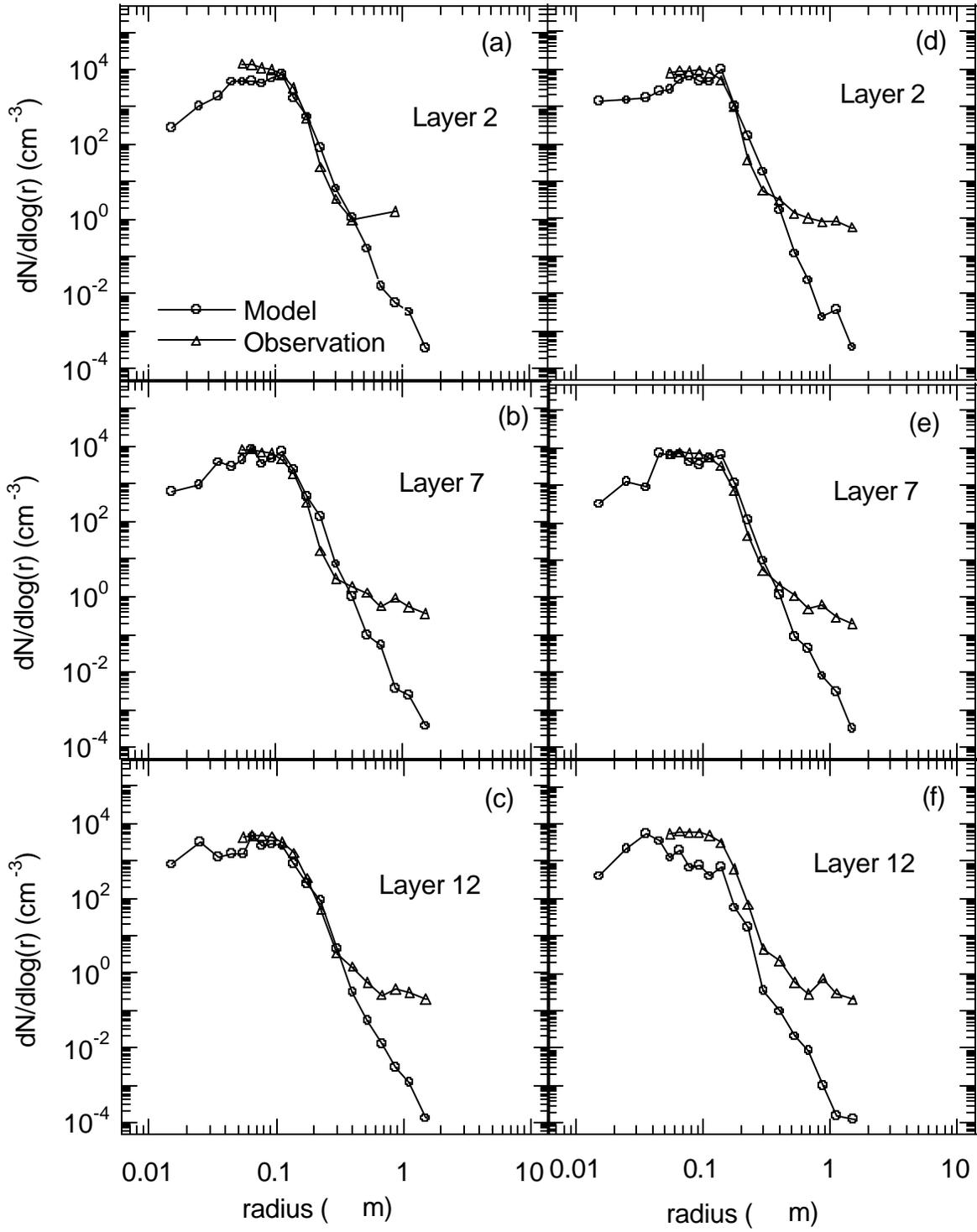


Figure 11

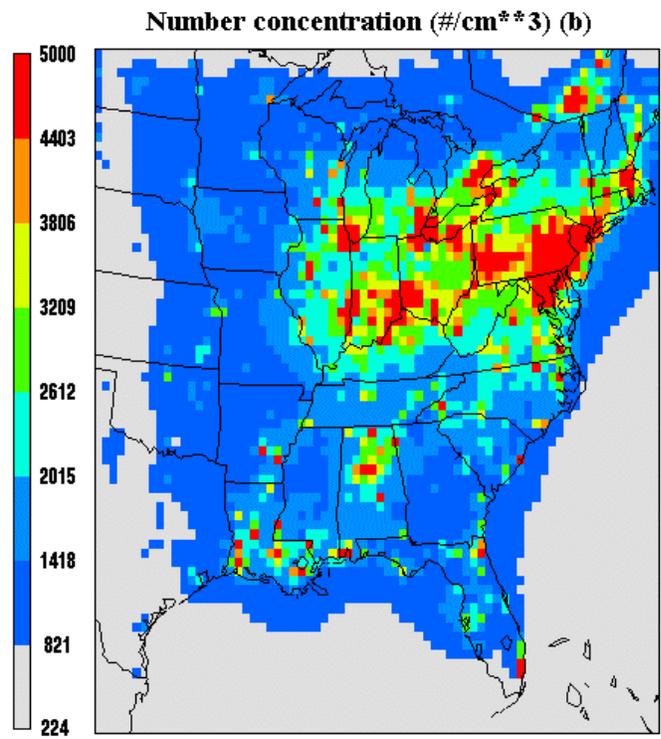
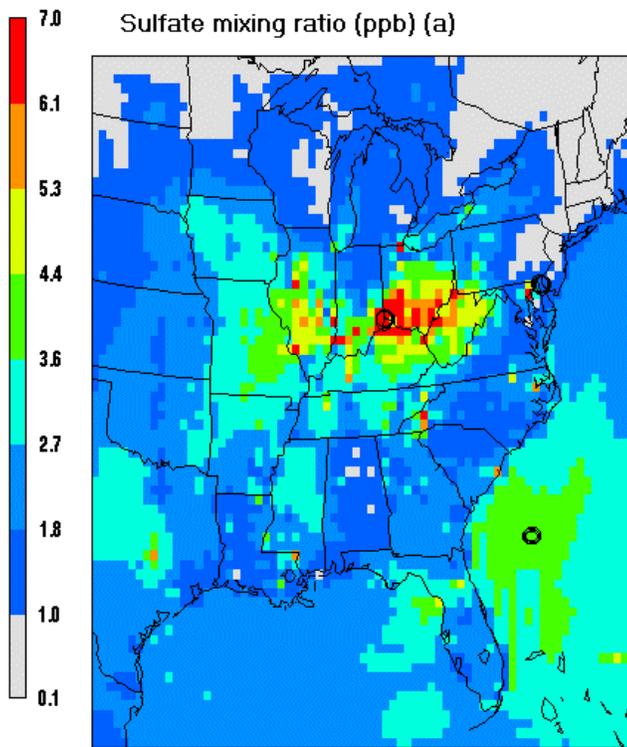


Figure 12

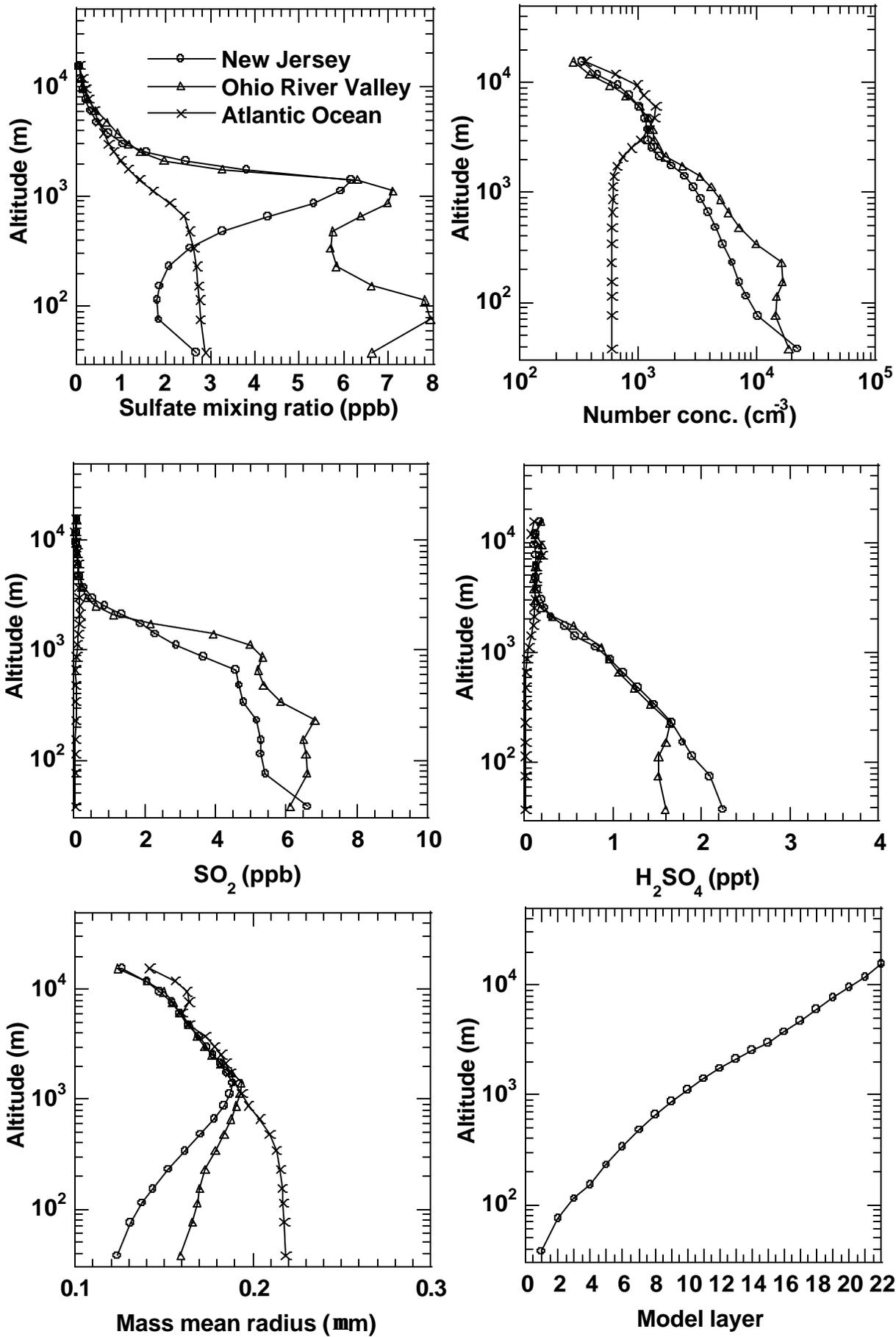


Figure 13